

Rolling 30 00
 Total \$2832 00

Length 5200 feet.

13988

1

E. D. Garwood ^{art} 1/2	11	X
J. W. Embrey sledge	11	X
Pearl Garwood	1 1/2, 1/2, 1/2	1X
Marion Shella barger, H. ch.	11	X
Peter Hudson wagon	11	X
Blaine Heath	11	X
H. R. Richey R. ch.	11	X
James Reams	1/2	X
Elmer Johnson	1/2, 1 1/2, 1/2, 1/5	X
F. J. Reams	1/2	X
Don Wonders III	11	X
Dticoll Wonders II	11	X
Don Lippincotts Rig		X

Road to Jefferson Perry

Bristle Ridge Pike 9/24/06

B.M.	5.49			29.95	29.00
X					
0	5.70		.21	29.74	29.74
S. side walk	6.50		.80	28.94	
1	4.00	2.50		31.44	30.50 ⁰⁴
S.S.W.	4.60		.60	30.84	
2	6.50		1.90	28.94	28.74 ⁰⁴
N.S.W.	7.00		.50	28.44	
S.S.W.	6.40	.60		27.04	
3	8.60		2.20	26.84	26.0
A.T.P.	0.98	10.48		1.83	24.96
X					
B.M.	3.50		2.52	22.44	
4+58 N.S.W.	4.30		.80	21.64	
5	3.85	.45		22.09	21.50 ⁰⁴
6	4.80		.95	21.14	21.25
7	5.00		.20	20.94	21.00 ⁰⁴
8 T.T.	7.79	6.01		1.01	19.93
X					
S. End 42" pipe	9.70		1.91	18.02	
9	7.10	2.60		20.62	24.50
	14.26	23.59	6.15	15.48	9.33
				6.15	
				9.33	

B.M. a cement walk of Ballinger's front porch.
 - Sta 5 into Ballinger pike in E. Lib.
 Angle N. 79° 00' W.
 - 00 side stance 30' to Left .00
 - 01 + 42 E. line of school lot.
 - 14 Sta 2+71 line Ballinger and Ballinger
 - 54 Sta 3+46 line Ballinger and Shellabarger
 - 74
 - 146
 - 54 + 55 line Shellabarger and Tregley
 - B.M. @ Shellabarger's porch floor
 - 57
 - 74 + 36 W. line school lot .06
 - 8+40 to Road + Line on NW. 2.07
 - Sta 0 Ang. N. 77° 15' W.
 - Sta 23 in @ old road
 - Sta 9+74 line Ball and Cemetery. 3.88

C

F

	7.10			20.62		Sta 10. Ang. N. 73° 30' W.	
10	4.50	2.60		23.22	27.20		3.78
T.P.	13.00	0.26	4.24	27.46			
π						Sta 11. Ang. N. 59° 00' W.	
11	8.90	4.10		31.56	32.00		.44
12	1.55	7.35		38.91	36.00	2.71	
						Sta 12 + 50' cemetery Gate.	
13	0.70	.85		39.76	40.00		.24
14	0.60	.10		39.86	40.50		.64
15 T.P.	12.58	1.08	48	39.38	39.90		5.2
π							
B.M.	7.96	2.62		42.00		B.M. Top Josiah's headstone oppo	
16	13.20		3.24	38.76	40.10		1.34
						Sta 16 + 60' Line Bell's Cemdry. N.	
17	12.40	.80		39.56	40.30		.74
18	10.80	1.60		41.16	42.90		1.94
19	6.40	4.40		45.56	45.50		
197.85	3.00	3.40		48.96		1785 a Bell's driveway	
	32.68	4.34	32.06	3.72	18.34		
	4.34		3.72				
	18.34		28.34				

C

F

	3.00			48.96			Sta 20. Ang. N. 87° 00' W.	
20	3.60		.60	48.36	47.80 ^{ch}	1.36	20+70' 12' to bank on N.	
21	8.00		4.40	43.96	46.50 ^{ch}			2.54
22	9.20		1.20	42.76	46.75			3.99
							22+50' Flat top-span	
23	7.60	1.60		44.36	47.00 ^{ch}			2.64
24	5.20	1.40		46.76	51.00 ^{ch}			4.24
T.P.	12.15	1.10	4.10	50.86				
∩								
25	8.50	3.65		54.51	55.90			1.39
T.P.	9.64	0.57	7.93	62.44				
∩								
26	8.40	1.24		63.68	60.80	2.88		
B.M.	4.56	3.84		67.52			B.M. 12" Walnut. N. 27	
27	4.77		.21	67.31		1.61	Sta 27 Ang. N. 97° 15' W.	
					65.70 ^{ch}			
28	3.30	1.47		68.78	68.00 ^{ch}	.78		
29 T.P.	12.70	1.78	1.52	70.30	72.70 ^{ch}		Sta 29+59' Line Bell rd & Armstrong rd	N. 4 2.40
T	24.79	3.45	2.75	6.41	21.34		Extingham rd & Armstrong. S.	
	3.45		6.41					
	21.34		21.34					

C

F

	12.70		70.30		
30	8.20	4.50	74.80	77.76	2.96
31	1.10	7.10	81.70	82.82	.92
T.P.	12.72	0.79	.31	82.71	
∇					
32	6.90	5.82	88.03	87.88	.15
B.M.	3.95	2.95	90.98		B.M. 10" Walnut, N. 32.
33	1.30	2.65	93.63	92.94	.69
T.P.	11.16	0.45	.85	94.48	
∇					
34	7.30	3.86	98.34	98.00 ^u	.34
35	2.70	4.60	102.94	103.20 ^u	.26
T.P.	11.50	0.69	2.01	104.95	
∇					
36	8.40	3.10	108.05	108.80	.25
37	3.60	4.80	112.85	113.34	.45
T.P.	11.77	1.05	2.55	115.40	
∇					
38	9.80	1.97	117.37	118.20	.93
B.M.	5.06	4.74	122.11		B.M. 18" Sugar, N. 38
39	4.80	.26	122.37	123.30	.93
	59.85	7.78	52.07	0.00	
	7.78				
	52.07				

	4.80			122.37		
T.P.	12.88	0.49	4.31	126.68		
X					155.22	
40	12.20	.68		127.36	128.00	.64
41	7.80	4.40		131.76	138.00	1.24
42 T.P.	12.67	2.70	5.10	136.86	138.00	1.14
X						
43	6.90	5.77		142.63	143.00	.37
44	2.80	4.10		146.73	146.25	.02
T.P.	6.65	0.47	2.33	149.06		
45	5.60	1.05		150.11	150.50	.49
450	3.75	1.85		151.96		
B.M.	3.70	.05		152.01		
46	4.10		.40	151.61	151.00	.61
47	5.10		1.00	150.61	149.75	.86
48	7.80	2.70		147.91	148.50	.59
T.P.	9.20	9.85	2.05	145.86		
49	10.90	1.70		144.16	147.25	3.09
	46.20	24.41	29.64	7.85	21.79	
	24.41					
	21.77		7.85			
		21.77				

sta. 45 Ang N. 76° 30' W

B.M. 24 Oak near 44. S.

	10.90			144.16			
50	11.70		0.80	143.36	145.00	5x7.90' Wooden box Cul. 18" x 24"	2.64
B.M.	11.10	0.60		143.96		B.M. 30" White oak N. 50+50'	
51	9.50	1.60		145.56	148.00		2.44
52 T.P.	5.42	5.26	4.24	149.80	152.32		2.52
T.P.	12.01	1.50	3.92	153.72			
53	9.80	2.24		156.36	156.64		2.8
54	9.60	0.20		161.58	160.96	62.5+7.36 @ Armstrong Gate	2.9
54+55 ^{OTT} At gate (house)	2.04	7.56		164.26	161.04	51.5+5.5' Ang. N. 73° 15' W. (Armstrong's house)	
55	4.30		2.26	165.26	161.28		
56 T.P.	8.62	10.42		6.12	155.89	158.75	2.86
57	10.10		6.98	153.94	156.12		2.18
+90 Bridge floor	9.40	1.60		154.53		Bridge 18' span	
B.M.	10.32		1.92	153.61		B.M. on N.W. cor. N.W. abutt.	
58	9.40	.42		154.94	153.50	1.44' of bridge on cement coping.	
59	7.00	2.42		156.93	157.35		4.2
	36.95	24.18	29.65	11.88	12.77		
	24.18		11.88				
	12.77		12.77				

See Relevel notes.

C

F

	7.00			156.93	
60 T.P.	13.00	3.20	3.80	160.73	161.20 ^{ch}
61		9.90	3.10	163.83	165.90
62		6.00	3.90	167.73	170.60
63 T.P.	10.86	0.80	5.20	172.93	175.30
63+35	(near gate)	4.30	6.56	179.49	
64		4.10	.20	179.69	180.00
T.P.	8.82	1.85	2.25	181.94	
65		6.60	2.22	184.63	184.70 ^{ch}
66 T.P.	11.85	1.74	4.86	189.39	189.05
B.M.		5.63	6.22	195.24	
67		7.30	1.67	194.57	193.40 ^{ch}
68		4.20	3.10	196.97	197.75 ^{ch}
69 T.P.	12.31	1.40	2.80	199.87	200.40 ^{ch}
	51.53	8.99	4.21	42.54	
	5.99		1.67		
	42.54		42.54		

61+90' line Armstrong^{and} Williams S. 25.67

Williams yard gate

62 Sta. 61. line Armstrong^{and} Johnson N. 31
(stone on line)

34 Sta 66+69' W. cor. school lot.
B.M. 30" Walnut S. 66+50'

77

1.47

2.87

2.37

.07

.81

-.56

				C	F
	12.31		199.47.		
70	7.90	2.41	201.88	203.50 ^{ch}	1.62
71	7.40	2.50	204.81	206.65	1.84
72	5.10	2.30	207.07	209.80	2.73
73 T.P.	12.10	1.30	211.21	212.95	1.74
74	7.40	4.76	215.57	216.10	.59
75	5.40	2.00	217.57	219.25	1.74
76 T.P.	10.71	2.00	220.97	222.40 ^{ch}	1.43
77	5.00	5.91	226.49	226.65	1.16
78 T.P.	11.45	1.01	230.48	230.90 ^{ch}	.42
79	8.40	3.05	233.53	232.95	
B.M.	4.01	4.39	237.92		
	46.77	8.32	38.45		
	8.32				
	<u>38.45</u>				

B.M. 30" oak S. 79+40.

	4.01			237.92		
80	5.00	0.99		236.93	235.00 ^{ch}	1.93
81	6.00	1.00		235.36	236.29	07 Bl + 4 line Johnson ^{2nd} Stewart. N.
+50	6.60	0.60		235.33		Argo's drive.
82	7.40	0.30	0.50	234.92	237.58	
+36	7.10	0.30		234.83		12 Box. (Top)
83	5.60	1.50		236.33	238.87	2.66
						2.54
54	3.60	2.00		238.33	240.15 ^{ch}	1.82
85 TP	10.83	0.86	2.74	241.07	243.15 ^{ch}	85 + W. line Argo ^{2nd} Johnson. S. 2.08
Σ	25.90					
86	7.20	3.63		244.70	247.15 ^{ch}	86 + 70' Stewarts Drive way 2.45
87	2.50	4.70		249.40	252.15 ^{ch}	87 + 21' R.F. Johnson's " " 2.75
T.P.	12.78	0.44	2.66	257.46		
Σ	267.24					
88	7.10	5.68		257.14	257.60	88 + 50' Bank on each side .76
T.P.	12.88	0.38	6.72	263.86		
Σ	276.34					
89	10.60	2.28		266.14	263.05 ^{ch}	3.09
	40.50	12.28	31.61	3.39	28.22	
	12.28		3.39			
	28.22		28.22			

	10.60			266.14	
90	10.20	0.40		266.54	267.05
91	8.20	2.00		268.54	271.05
B.M.	4.31	3.59		272.43	
92	4.50		0.19	272.24	275.05
T.P.	11.26	0.26	4.24	276.48	
Σ	287.74				
93	6.80	7.46		280.74	279.05 ^{ch}
94	5.20	1.60		282.54	283.05
95	4.20	1.00		283.54	285.94 ^{ch}
96	1.60	2.60		286.14	288.88
T.P.	11.92	0.95	0.65	286.77	
Σ	298.71				
97	8.60	3.32		290.11	292.03
98	2.05	6.55		296.66	295.23 ^{ch}
99	1.60	.45		297.11	297.50 ^{ch}
	33.78	2.81	31.16	30.97	
	2.81	.19	0.19		
	30.97	30.97			

11

F

Sta 90. Ang. N. 79°15' W. .51

do + 95' Line. Stewartnd Reams 2.51

B.M. White ash N. 91+75' .115

Sta 91+65' Line Johnsonnd Reams. 2.81

289

44+50' Box culvert 9" x 14" .51

2.40

2.69

1.92

1.43

.39

	1.60			297.11	
100	2.10		0.50	296.61	297.90
101	1.90	0.20		296.81	298.30
T.P.	6.22	1.95	0.05	296.76	
Σ	<u>302.98</u>				
102	4.70	1.52		298.28	298.70 ^{ch}
103 ^{ch}	5.16	0.78	0.46	297.82	297.00 ^{ch}
104	7.30		2.14	295.68	294.00
105 T.P.	1.36	10.68	3.28	292.40	291.00 ^{ch}
Σ	<u>293.76</u>				
B.M.	3.62		2.26	290.14	
106	9.40		5.98	284.36	287.45 ^{ch}
107	11.60		2.20	282.16	283.50
T.P.	7.85	12.06	0.46	281.70	
Σ	<u>286.55</u>				
108	8.40		3.55	278.15	281.00 ^{ch}
109	9.30		0.20	277.25	281.75 ^{ch}
	14.03	33.89	1.72	21.58	19.86
		<u>14.03</u>		<u>1.72</u>	
		19.86		19.86	

10750' Box culvert 5'x12" 1.29
 1.49
 42
 32
 1.68
 7-40 10.105 line Jeffersonrd & Perry Tp.
 B.M. 30' White oak N. 105+50'
 2.89
 1.37
 2.85
 5.
 4.50
 2.85
 5.
 4.50

C

F

	9.30			277.25	
110 ^{old} _{TP}	3.94	5.36		282.61	284.00
T.P.	11.38	0.72	3.22	285.83	
Σ	297.21				
111	4.90	6.48		292.31	292.25
T.P.	7.50	0.07	4.83	297.14	
Σ	304.64				
112	4.20	3.30		300.44	297.50 ^{ch}
113	3.88	.32		300.76	300.75 ^{ch}
114	4.60		.72	300.04	300.70 ^{ch}
115	4.70		.10	299.94	300.70 ^{ch}
116	3.90	.80		300.74	299.50
117 T.P.	3.57	4.80	.90	299.84	298.25
Σ	303.41				
B.M.	2.36	1.21		301.05	
118	9.30		6.94	294.11	294.00 ^{ch}
119	8.80	.50		294.61	299.00 ^{ch}
	31.75	14.37	26.02	8.66	17.36
	14.39		8.66		
	17.36		17.36		

2.94 Sta. 112+39' Hing. N. 79° 45' W.
 -01
 Sta. 115. Hing. S. 84° 00' W.
 2.24 115+10' Box culvert 14" X 18"
 4.59 116+62' @ Jamison Road, N.

B.M. Door sill Watkins house
 113+75' Tile culvert 18"
 118+85' Box " " 16" X 20"

4.39

.36

.81

2.89

4.39

C

F

	8.80			294.61	303.50		
120	3.60	5.20		299.81	304.00		4.17
T.P.	13.00	2.31	1.29	301.10			
T	314.10						
121	5.50	7.50		308.60	308.35	.25	
T.P.	9.56	0.32	5.18	313.78			
T	323.34						
B.M.	6.52	3.04		316.82	312.70		B.M. 24" Black Walnut N. 121+30'
122	8.60		2.08	314.74	312.70	2.04	122+25' Ang. S. 85° 00' W.
123	5.00	3.60		318.34	317.05	1.29	
124	4.80	0.20		318.54	318.50		.04
125	4.70	0.10		318.64	318.25	.39	
126	7.60		2.90	315.74	318.34		126+60' Box Culvert 12" 2.60
127	7.20	0.40		316.14	318.42		2.28
128	5.00	2.20		318.34	318.50		.16
129 T.P.	11.40	3.32	1.61	319.95	320.00		.05
T	331.35						
	31.36	6.02	30.32	498	25.34		
	6.02		4.82				
	25.34		25.34				

	11.40			319.95		
130	11.40	0.00		319.95	321.50	1.55
131	10.20	1.20		321.15	323.00	1.85
132	7.40	2.80		323.95	324.50	1.55
B.M.	3.34	4.06		328.01		
133	3.60		0.26	327.75	326.00	1.75
134	7.80		4.20	323.55	325.00	1.45
B.M.	7.98		0.18	323.37		
135	6.80	1.18		324.56	327.50	2.95
136	1.80	5.00		329.55	330.00	1.45
T.P.	13.00	0.87	0.93	330.48		
Σ	343.48					
137	10.30	2.20		332.68	334.00	1.32
138	6.80	4.00		336.68	338.00	1.32
139	2.90	3.90		340.58	342.00	1.42
T.P.	11.81	0.82	2.08	342.66		
Σ	354.47					
	24.40	1.69	2.35	4.64	22.71	
	1.69		4.64			
	22.71		22.71			

Sta 132 Ang. S. 84° 15' W.
 B.M. N.W. of Reams Well Platform.

134+40', 12" pipe culvert.
 B.M. 36" white oak. S. 135

139+90' line Reams^{9th} Mrs Ball, N.

	6.77			361.92			
150	3.30	3.47		365.39	368.00	2.37	
151	6.20		2.90	367.49	361.75	74	151.746 line. Clapsaddle 9 th school lot. S. —
B.M.	7.42		1.12	361.27			B.M. N.W. cor doorsill of schoolhouse
152	9.80		2.38	358.89	360.50		152.760 line Clapsaddle 9 th Adams S. 1.61
153	12.60		2.80	356.09	359.25		153. Adams lane
o Lane	15.50		2.90	353.19			153.775 Curle's lane 3.16
154	12.20	3.30		356.49	357.00		154. 12" x 12" Box culvert: .57
155	10.40	1.80		358.29	361.35		3.06
156	10.16	5.70	4.70	362.99	368.70		.91
T	<u>37315</u>						
157	7.30	2.88		365.85	366.05		157. Ang. S. 87° 15' W. 1.20
158	5.40	1.90		367.75	368.40		.65
159	4.70	0.70		368.45	369.00		159.790 o Clapsaddles yard gate .55
B.M.	1.59	3.11		371.56			B.M. Door sill w door in front (clapsaddles)
	1693	7.29	21.84	12.20	9.64		
	7.29		12.20				
	<u>9.64</u>		<u>9.64</u>				

See Changed Line of June 18.

	1.59				371.56				
160	5.10		3.51	368.05	368.05	-05	160.20 Ang. N. 84° 15' W.		
161	7.60		2.50	365.55	365.80				.25
162	10.10		2.50	363.05	363.60		162.75 ± 14" X 12" Box culvert.		.55
163	10.00	0.10	0.10	363.15	363.40				.25
164	9.10	0.90		364.05	363.20	.55			
165	TP. 6.05	9.70		0.80	363.25	363.50			.25
	<u>7</u>	<u>367.30</u>							
166	5.50	0.55		363.80	363.80	.00			0.0
167	6.70		1.20	362.60	363.00				.40
168	7.10		0.40	362.20	363.50		168. Ang. N. 87° 15' W		1.30
169	6.40	0.70		362.90	364.00				1.10
	7.14	16.30	2.25	10.91	8.66				
		<u>7.64</u>		<u>2.25</u>					
		8.66		8.66					

C

F

	6.40		362.90		
170	5.00	1.40	364.30	364.60	.30
171	4.40	0.60	364.90	365.20 ^{ch}	.30
172	3.10	1.30	366.20	364.70 ^{ch}	
173	10.30	7.20	359.00	362.10	3.00
174	12.80	2.50	356.50	359.30	2.80
T.P.	5.50	12.81	0.01	356.49	
T	361.99				
175	6.10	0.60	355.89	356.60 ^{ch}	.71
176	5.80	0.30	356.19	356.80	.61
177	3.30	2.50	358.69	357.00 ^{ch}	1.69
178	8.30	5.00	353.69	354.70	1.01
179	11.40	3.10	350.59	352.40	1.81
B.M.	9.55	1.85	352.44		
	11.98	22.36	18.41	10.46	
		11.80	7.95		
		10.46	10.46		

150 Sta 172+36' Ang. S 80° 30' W.
 172+75' line clapsaddle 2nd Farney S.
 clapsaddle 2nd Elliot N.

From sta 175 side stakes
 30' to N.

Elliot Gate way, N.

Sta 175+63 1/2 Ang. S 81° 30' W.

B.M. S.E. L lower step Elliott's ranch.

	9.55			352.44	
180	13.30		3.75	348.69	355.10 ^{ch}
181	13.20	0.10		348.79	350.84
182	9.60	3.60		352.39	351.57
183 T.P.	0.77	8.67	0.93	353.32	352.30 ^{ch}
∇	<u>357.11</u>				
184	3.60		2.81	350.51	350.15
185	6.00		2.80	348.11	348.00 ^{ch}
186	9.70		3.70	344.41	344.20
T.P.	2.10	12.50		2.80	341.61
∇	<u>343.71</u>				
187	4.40		2.30	339.31	340.00
188	10.60		6.20	333.11	335.20 ^{ch}
189	10.20	0.40		333.51	336.00
12A4	31.37	5.03	23.96	18.93	337.00
	<u>19.44</u>		5.03		
	18.93		18.93		

					1.41
					2.05
					82
182	Sta 183	Ang.	S. 78° 15' W.		
					Bank on N. between 185 & 186
					36
	11	186 + 22	Ang.	S. 66° W.	
					41
					151 + 27' Ang. S. 61° 30' W.
					157 + 22' line Fromme and Piper
					158 + 36' Stone culvert 9' x 19'
					2.89

	10.20			333.51	337.00
170	7.50	2.70		336.21	338.50
B.M.	2.20	5.30		341.51	
191	5.40		3.20	338.31	339.70
192	2.10	3.30	2.30	341.61	341.40
193	0.90	1.40		343.01	343.10
T.P.	5.33	0.73	0.08	342.98	
T	<u>348.31</u>				
194	4.40	0.93		343.91	343.94
195	5.60		1.20	342.71	344.78
196	5.60			342.71	345.62
197	4.10	1.50		344.21	346.46
198	0.10	2.00		348.21	347.80
T.P.	4.14	0.27	2.17	348.07	
T	<u>352.78</u>				
199	4.40		0.26	347.78	348.14
	19.67	5.40	19.13	5.86	14.27
	5.40		5.86		
	<u>14.27</u>		<u>14.27</u>		

1907 90' Stanley's Drive
B.M. 30" Walnut N. 1907 90'



112+45' of pipe Drive.

177+92 Ang - S. 63° 45' W
Line Ripery and Garwood. S.

99+50 Ang - S. 78° 30' W.

30'-7" to pole

1.79

1.39

-0.9

.03

2.07

2.91

12.25

.36

	4.40			347.78	
200 ^{old} T.P.	8.07	1.33		349.11	348.95
201	5.10		2.03	347.08	347.50
202	4.80	0.30		347.38	348.65
203 T.P.	2.24	3.55	1.25	348.63	348.60
Σ	350.87				
204	2.08	0.16		348.79	349.15
205	4.50		2.92	346.37	346.10
B.M.	5.00		0.50	345.87	
206	5.94		0.94	344.93	343.05
207	7.80		3.86	341.07	340.00
T.P.	0.58	12.97		317.33	37.90
Σ	336.48				
208	1.90		1.32	336.58	334.70
209	7.70		5.80	330.78	328.70
T.P.	0.26	13.25		5.55	325.23
Σ	325.49				
210	7.22	29.77	3.04	25.59	22.55
		7.22		3.04	
		22.55		22.55	

201. Ang - S. 74° 00' W.

201 @ Elmer Johnson. yard gateway. 42

67

204 + 6 E line Johnson and Maddox. N. 36

27 205 + 55 line Garwood and Maddox. S.

B.M. 15' Walnut. S

209. Ang - S. 83° 00' W.

	0.26			325.23		
210	3.60		3.34	321.89	322.70	.81
211	10.70		7.10	314.79	316.70 ⁴⁶	1.91
T.P.	0.11	13.00	2.30	312.49		
Σ	312.60					
212 ^{.4} T.P.	3.38		3.27	309.22	312.35	3.18
213	8.30		4.92	304.30	308.00 ⁴⁶	3.70
214	10.50		2.20	302.10	305.10 ⁴⁶	2.90
215	10.90		0.90	301.70	302.65 ⁴⁶	.95
216	10.30	0.60		302.30	302.65 ⁴⁶	.35
217 T.P.	5.05	9.24	1.06	303.36	307.00 ⁴⁶	.64
Σ	308.41					
218	5.80		0.75	302.61	303.71 ⁴⁶	1.29
219 ^{old} T.P.	6.44		0.64	301.97	303.60 ⁴⁶	1.63
	5.42	28.68	1.66	29.92	23.26	
		5.42		1.66		
		23.26		23.26		

213 + 19 Ang - S. 76° 30' W.

218 Ang - S. 80° 15' W.

219 + 82' Ang. N. 59° 30' W.

	6.74		301.97			
220	4.70	1.74	303.71	303.30		
221	5.30		0.60	303.11	308.00	
222	10.50		5.20	297.91	299.00	222 + 30' Ang. N. 85° 00' W.
T.P.	1.52	13.20	2.70	295.21		
Σ	296.73					
223	3.50		1.98	293.23	295.00	1.77
224	4.70		1.20	292.03	291.00	224. Angle N. 75° 30' W.
B.M.	3.20	1.50		293.53		B.M. 12" Lacust. S. 224 + 50'
225 T.P.	0.12	11.38	8.18	285.35	285.45	1.10
Σ	285.47					
226 T.P.	6.78		6.66	278.69	278.65	1.16
227 T.P.	0.24	12.66	5.88	272.81	272.25	
Σ	273.05					
228	8.20		7.96	264.85	266.00	Bank on S. 228
T.P.	0.16	13.18	4.98	259.87		1.15
Σ	260.03					
229 (old T.P.)	1.31		1.15	258.72	259.75	1.03
	8.48	51.73	324	46.49	43.25	
		8.49		3.24		
		43.25		43.25		

0.40
1.30
2.30

F

	1.31		258.72		
230	9.00	7.69	251.03	253.50	2.47
T.P.	0.55	13.05	4.15	246.98	
X	<u>147.53</u>				
231	32.0	2.65	244.33	247.25	2.92
232	7.60	4.40	237.93	241.50	1.07
233 T.P.	0.14	11.34	3.74	236.19	234.75
X	<u>236.33</u>				
234 (old)	6.65	6.51	229.58	228.50	234+84' Ang. N. 75° 30' W.
T.P.	0.49	12.90	6.25	223.43	234+94' line Maddox & Williams S.
X	<u>223.92</u>				
235 old T.P.	2.46	1.97	221.46	222.25	1.79
236	10.00	7.54	213.92	214.20	28
T.P.	0.46	13.25	3.28	210.64	
X	<u>211.10</u>				
237	3.15	2.69	207.95	206.15	25
238 old T.P.	9.66	6.51	201.44	198.20	3.34
T.P.	0.07	12.85	3.19	198.25	
X	<u>198.32</u>				
239	5.22	5.15	193.10	190.65	239+19' Ang. S. 82° 45' W.
T.P.	0.13	15.05	7.83	185.27	
X	<u>185.40</u>				
	3.02	96.47	73.45	73.45	
		3.12			
		73.44			

	0.13		185.27			
240 ^(old) T.P.	- 2.89	2.76	182.51	182.25	251 240 - Ang. S. 76° 45' W.	
T.P.	0.68	13.03	10.14	172.37		
Σ	<u>173.05</u>					
241 T.P.	3.20	2.52	169.85	170.20		25
T.P.	-0.03	12.10	8.90	160.95		
Σ	<u>160.92</u>					
242 ^(old) T.P.	3.72	3.75	157.20	158.45		1.20
T.P.	0.28	12.89	9.17	148.03		
Σ	<u>148.31</u>					
243 ^(old) T.P.	2.36	2.08	145.95	146.60		.65
T.P.	0.52	13.27	10.91	135.04		
Σ	<u>135.56</u>					
244 ^(old) T.P.	3.62	3.10	131.94	134.80	244 + 35' - Ang. S. 89° 00' W.	2.86
T.P.	0.54	13.26	9.64	122.30		
Σ	<u>122.84</u>					
245	2.50	1.96	120.34	123.00	245 line Williams and Grubbs	2.66
246 ^{T.P.}	0.76	12.34	9.54	110.80	246 x 25' - 6' plank bridge	2.50
Σ	<u>111.26</u>					
247 ^(old) T.P.	11.09	10.33	100.17	103.25		2.88
T.P.	0.33	13.08	1.99	98.18		
Σ	<u>98.46</u>					
248	5.10	5.22	92.96	93.20	248 boulders on S. of 245	.04
	3.26	15.57	92.31	92.31		
	<u>93.31</u>					

	5.60			92.96	
T.P.	1.35	12.61	7.01	85.95	
∇	87.20				
249 ^{OH} (T.P.)	5.72	6.49	4.37	81.58	83.60
T.P.	0.41	13.24	7.52	74.06	
∇	74.37				
B.M. Grubb's yard gate	4.70		4.29	69.77	
	5.00		0.30	69.47	
250	5.74		0.74	68.73	73.00 ^{OH}
251 T.P.	4.92	11.80	6.06	62.67	69.00 ^{OH}
∇	67.49				
252	5.40		0.48	62.19	64.30
253	4.90	0.50		62.69	61.60 ^{OH}
B.M.	5.48		0.58	62.11	
B.M.	5.66		0.18	61.93	
Bridge floor Chan. Mad River	4.76	0.90		62.83	
	13.20		8.44	54.39	
254	5.49	7.71		62.18	61.60 ^{OH}
255	6.96		0.47	60.83	62.00 ^{OH}
256	6.70	0.26		60.89	61.70
257	6.44	0.26		61.15	61.40
258 T.P.	4.33	6.48	0.04	61.71	61.10 ^{OH}
∇	65.34				
	12.28	44.13	9.63	41.48	31.55
		12.28		9.63	
		31.95		31.95	

B.M. N.E. L Doorstone (Grubb's)
OPP 249+90

250+37' Angle. N. 87° 15' W. 4.27
4.30

252+30' Ang. N. 61° 45' W. 2.71
(E. Mad River bridge)
252+40' O Mad River bridge

B.M. N.E. L N.E. Wing Wall Bridge
B.M. S.E. L W. Abut. on H.B

change this floor Elev 62.83

1.42

1.37

.81

.25

	7.33			61.11		
259	4.50		0.17	60.94	60.60	Sta 259+29'. T & O. C. R. R. switch
260	4.40	0.10		61.04	61.00	Sta 260+46' Ang. N. 62° 00' W
259+29	4.10	0.80		61.34		
261	4.50	.00	.40	60.94	60.70	
262	5.00		0.50	60.44	60.40	Sta 262+30 1/2' Ang. N. 70° 15' W. 262+60'. Wonders Lane N.
263	4.00	1.00		61.44	61.70	Sta. 263 three nails around spike in W. plank of bridge over Penrock ditch.
chan. Penrock ditch	11.10		7.10	54.34		
264	3.00	8.10		62.44	63.00	263. Angle. N. 88° 15' W.
T.P.	7.13	0.26	2.74	65.48		
Σ	74.21					
265	7.90	1.23		66.41	65.40	
266	4.50	3.70		69.81		Sta 267+46' End of pike in O
267	3.10	1.40		71.21		W. L. Z & R. pike in Zanesfield.
+66'	2.20	0.90		72.11		
B.M.	1.24	0.96		73.07		B.M. S. E. door-sill N. door E side McAtco's house
266 N. sidewalk	4.20		2.96	70.11		
266 S " "	4.80		.60	69.51		
267 N. " "	2.60	2.20		71.71		
" S " "	3.60		1.20	70.51		
N. Walk	2.50	1.30		71.81		
S. Walk	3.15		0.65	71.16		
Σ	13.46	7.65	13.58	10.05		E. Side Main St.

Side Walk Notes in E. Liberty

	S. side	N. side
1	19'-6"	17'-8"
2	19'-10"	17'-11"
3		17'-4"
4		20'

Measurements to outer edge
of walks.

8152 48" iron pipe 20' to S. - 30' to N.

Side Walk Notes in Zanesfield

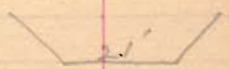
265	17'-6"	21'-0"
266	18'-0"	20'-8"
267	20'-0"	21'-6"

253 Grade 10'

257+60 " 15'



121 cut 21' wide



54		156.13
X	6.00	<u>162.13</u>
+55	3.40	158.73
By gate	2.20	159.93
55	5.70	156.43
53	11.10	151.03
56	11.80	150.33
Bridge of 4000	12.70	147.43

Relevel 6/22, 06.

42 T.P.	12.23	136.86
Σ	<u>149.09</u>	
43	6.30	
44	2.40	
T.P.	6.41 0.00	149.09
Σ	<u>155.50</u>	
45	5.40	
+50	3.60	
B.M.	3.54	151.94
46	4.00	
47	5.00	
48	7.60	
49	11.40	
+75	12.80	
T.P.	11.37 12.30	143.20
Σ	<u>154.57</u>	

B.M. Oak Jo's.

Σ	<u>154.57</u>		
50	11.30		
B.M.	10.51		
51	9.00		
52	4.70		
T.P.	10.78	-0.01	154.58
Σ	<u>165.36</u>		
53	9.00		156.36
54	3.78		161.58
+55	1.10		164.26
8 ^{neg} gate	0.10		165.26
55	3.50		161.86
56	11.15	9.47	155.89
Σ	<u>167.04</u>		
57	13.10		153.94
B.M.	9.37		157.67
Bridge g ¹⁰⁰⁷	12.30		154.74
58	12.10		154.94
59	10.00		157.04

Gate at 54+40

Top cap of post of handrail N.E. of bridge

T	<u>167.04</u>		
60		6.20	160.84
61		3.70	163.74
T.P.	<u>11.81</u>	0.20	166.84
T	<u>178.66</u>		
62		10.80	167.85
63		5.50	173.15
T.P.	<u>11.38</u>	0.00	178.65
T	<u>190.03</u>		
64		10.30	179.73
65		5.40	184.63
66	<u>11.25</u>	0.64	189.39
T	<u>200.64</u>		
67		6.50	194.14
68		3.70	196.94
69	<u>10.67</u>	0.80	197.84
T	<u>210.51</u>		

Σ	<u>210.51</u>		
70	8.40		202.11
71	5.70		204.81
72	3.50		207.01
T.P.	12.80	0.00	210.51
Σ	<u>223.31</u>		
73	12.10		211.21
74	7.80		215.51
75	5.80		217.51
76	2.40		220.91
T.P.	13.28	0.20	223.11
Σ	<u>236.39</u>		
77	9.70		226.69
78	5.70		230.69
79	2.60		233.79
T.P.	6.06	0.03	236.36
Σ	<u>242.48</u>		

	<u>242.42</u>	
⌘ B.M.	4.14	238.28
80	5.27	237.18
81	6.06	236.36
82	7.50	234.92
83	5.70	236.72
84	3.70	238.72
85 T.P.	1.00	241.42

Culverts (with Com. July 5 1888)

Zanesfield

5.30'	16'	10" pipe	Alley Approach
16'	at 249 1/2	10"	S.
36'	at 24		
16'	at 247+40	10"	S.
	Sta.		
+2'	245+25	36"	
Sta.			
236	40	10"	
232	40	12"	
223	36	10"	
218+80	36	10"	
212	16	10"	N.
About 224?	16	10"	S.
202	16	10"	N.
202+30	16	10"	S.
192+45	16	10"	S.
190+40	16	10"	N.
188+20	36	12"	
180+50	36	10"	
178	16	10"	N.
174	36	10"	
166+90	36	10"	
167	16	10"	N.

162+75	36	12"	
160+25	16'	10"	S.
154	36'	12"	
153+75	16'	10"	
146	36'	10"	
140+30	16'	12"	
134+40	36'	16"	
130	36'	10"	
126+60	36'	10"	
118+75	52	24"	
115	36'	12"	
108+15	48'	30"	
100+50	36'	10"	
95	36'	10"	
87+40	20'	10"	S.
86+70	20'	10"	N.
82+40	40'	24"	
81+50	16'	10"	S.
66+50	16'	10"	N.
64	16'	10"	S.
64	16'	10"	S.
53	16'	10"	S.

50 + 20	44'	24"	S
27 + 50	36'	12"	
22 + 50	42'	36"	
17	36'	10"	
12 + 50	24'	10"	N.
8	40'	16	
8	6"	48"	
M. Shellenbarr	16'	10"	N
4	16'	10	N

Culverts ^{- 7/20 06}

188+35 36' - 12"

Stakes 20' from 0

cuts

189	333.51		
X	2.90	336.41	
Inlet	4.20	332.21	
I.S.	3.22	333.19	332.20 1.00
Outlet	7.00	329.41	
O.S.	6.40	330.01	329.40 .61
O Road	3.50	332.91	

180+50 36' - 10"

Stakes 20' from 0

B.M.	362.44		
X	1.76	354.20	
Inlet	7.15	347.05	
I.S.	6.05	348.15	347.00 1.15
Outlet			
O.S.	6.18	348.02	346.50 1.52
O Road	5.40	348.80	

6.18
6.05
.13

Guy Garwood 11 X

Don Wonders 1

Driscoll Wonders 1

Grade

Inlet Sta.		332.21	
X	5.4	337.6	
Exp. I.	4.5	333.1	331.9
" O.	7.3	330.3	329.1.10

B.M. 273 - 352.44

X 354.67

O.S. 6.58 348.09

O.S. 6.45 348.22

10/2/06

found
stakes all ok

6.58
.13
6.45

174 36'-10" Grade Cuts
 20 from 0
 174 356.50
 X 4.30 ~~360.80~~
 inlet 5.10 355.70 Surface
 I.S. 3.97 356.83 North Level 1/12
 outlet 5.70 355.10 surface 35
 O.S. 4.64 356.16 3.55.02 1/16
 Level

166+80 36'-10"
 20' from 0
 165 TP 363.25
 X 2.88 ~~366.13~~
 inlet 3.80 362.33
 I.S. 2.83 363.30 360.50 2.80
 outlet good
 O.S. 4.02 362.11 360.00 2.11
 O Road 3.40 362.73

			Grade
173		359.10	
	2.34	361.34	
10" pipe	4.65	356.69	355.79
10" well	5.34	356.00	355.1
165		363.25	
X	4.3	367.55	
10" TP	6.2	361.85	360.45
10" Ot.	6.8	360.15	359.85

162 +67

36'-12"

20' from @

Cute

165

363.25

X

5.25 368.50

Inlet

8.20 360.30

I.S.

7.25 361.25

360.30

.95

outlet

10.10 358.40

O.S.

10.10 358.40

358.40

0.00

@ Road

5.70 362.50

8+27 36'-16"

20' from @

8

19.93

X

4.20 24.13

inlet

6.60 17.53

I.S.

5.30 18.83

17.50

1.33

outlet

8.30 15.83

15.80

16.20

0.03

@ Road

4.20

165

363.25

X

4.2

367.45

Top 12"

I.S. 6.4

361.05

359.97

Top 12"

I.S. 3.0

359.45

358.37

Grade

8

19.93

X

4.8

24.73

Top 16"

I.S. 6.2

18.53

17.13

Top 16"

I.S. 7.8

16.9

15.50

8+60

6'-48"

16+54

36'-10"

20' from 0

17

39.56

X

3.00 42.56

inlet

4.70 37.66

37.25

I.S.

5.35 38.71

37.50 1.21

outlet

6.60 35.96

O.S.

5.54 37.02

37.00 0.02

0 Road

3.40

22+57

42'-36"

23' from 0

22

42.76

X

3.50 46.26

inlet

7.10 39.16

I.S.

6.30 39.96

39.00 .96

outlet

8.10 38.16

O.S.

6.25 40.01

38.00 2.01

Flat top bridge

Remove bridge and 1 Wall

Cuts

17

39.56

X

4.1

43.66

Top 10"

Exc In.

5.5

38.16

37.26

Top 10"

Exc Ot.

6.2

37.46

36.56

22

42.76

No Paper

Grade

27+78 36' - 12"
20' from \odot

B.M.	67.52		
π	4.35	<u>71.87</u>	
I.S.	2.90	68.97	66.00 2.97
Surface	4.00		
Outlet road			
O.S.	5.06	66.81	65.50 1.31
Surf.	6.00	66.81	
o Road	4.00		

CUTS

Sta.	Rod.		Grade
B.M.		67.52	
π	5.11	<u>72.92</u>	
Top 12" Pipe In.	5.8	67.1	66.02
Top 12" Pipe Ot.	6.1	66.8	65.72

50+34 44' - 24"
24' from \odot

B.M.	143.96		
π	5.40	<u>149.36</u>	
Inlet	7.60	141.76	141.70 7.3
I.S.	6.73	142.63	
outlet	8.20	141.16	
O.S.	7.40	141.96	141.20 7.6
o Road	5.60		
	4.		

Sta.	Rod.		Grade
B.M.		143.96	
π	3.95	<u>147.91</u>	
Top 24" Pipe In.	4.6	143.3	141.2
Top 24" Pipe Ot.	5.0	142.9	140.8

82+30 40'-24"

22' from @

			Sta	Road	Grade
82	234.72		32		234.72
∩	4.73	239.65		1.6	237.32
inlet	5.50	234.15			
I.S.	4.41	235.24	34.10	1.14	234.10
outlet	7.20	232.45			
O.S.	5.46	234.19	32.45	1.74	232.45
○ Road	3.90				
avg's yard	3.20				

94+52 36'-10"

20' from @

			Sta	Road	Grade
94	282.54		94		282.54
∩	5.00	287.54		4.0	287.04
Surface	5.33	282.21			
I.S.	4.72	282.82	82.00	1.82	282.00
outlet	good				
O.S.	4.55	281.97	81.50	1.44	281.50
○ Road	4.40	283.4			

100 + 59

36' - 10"

20' from @

cuts

100	296.61		
π	4.90	<u>301.51</u>	
inlet	6.20	295.31	
I.S.	5.52	295.99	295.30 .69
outlet	7.00	294.51	2
O.S.	6.00	295.51	294.50 1.00
⊙ Road	4.70		

108 + 99.4"

48' - $\frac{30}{24}$ "

S. End 8' W. of Watkins + post on @

24' from @

109	277.25		
π	3.40	<u>280.65</u>	
inlet	7.20	273.45	
Surface	4.90		
I.S.	4.20	276.45	273.50 2.95
outlet	8.70	271.95	
O.S.	5.90	274.95	272.00 2.75
⊙ Road	3.40		

	Sta	Rod	Grade
100			296.4
π	4.7		<u>301.31</u>
TOP 10"			
Pipe In.	5.4		295.90
			295.0
TOP 10"			
Pipe OT.	6.2		295.10
			294.2

109

277.25

π

NO PIPE

115+11 36'-12"
 20' from \odot

114	300.04		
X	2.88	<u>302.92</u>	
Surface	2.50	300.42	
I.S.	1.76	301.14	298.25 2.91
outlet	7.00	295.92	
O.S.	5.72	299.20	296.00 1.20
\odot Road	3.20	299.72	

118+79
 52'-24"
 28' from \odot

118	1	<u>294.11</u>	
X	1.78	295.89	
inlet	4.90	290.99	291.00
I.S.	5.22	290.67	290.70 0.00
outlet	5.78	290.11	
O.S.	4.87	<u>291.02</u>	290.00 1.02
\odot Road	1.40		0.00

Sta	Rad.		Grade
114		300.04	
X	1.3	<u>301.34</u>	
Top 12" Pipe Inlet	5.2	299.1	298.02
Top 12" Pipe Outlet	7.0	292.34	296.26

118		294.11	294.11
X	4.3	298.41	
Top 24" Pipe Inlet	5.6	292.8	290.7
Top 24" Pipe Outlet	6.4	292.0	289.9

126+68 36'-10"
20' from @

126 315.74

π 4.54 320.20

inlet^{sup} 4.80 315.40

I.S. 3.95 316.35 315.50 .85

outlet 8.00 312.28

O.S. 5.77 314.31

@ Road 4.50

130+8

36'-10"
20' from @

130 319.95

π 7.20 307.15

inlet 8.10 19.05

I.S. 7.52 19.63

outlet 7.20 17.95

O.S. 8.30 18.85

@ Road 7.20

19.00 .63

18.00 .85

Sta. Rod Grade

127 316.14

π 4.2 320.34

Top 10" pipe Int. 7.4 315.94 315.04

10" S.W. Ot. 6.7 313.64 312.74

130 319.95

π 4.2

N.P.C

134+30 36'-16"
20' from @

B.M.
135 323.37

↑ 5.26 328.63

inlet 6.80 21.83

I.S. 5.92 22.71

outlet 13.00 15.63

O.S. 9.20 19.43

@ Road 5.60 323.03

21.80 .91

46.00

17.00 24.3

145+93 36'-10"
20' from @

146 352.12

↑ 4.50 356.62

inlet 5.60 351.02 South

I.S. 4.95 51.67

outlet 6.10 350.52

O.S. 5.16 51.46

@ Road 4.50

351.00 .67

350.60 .86

Sta Rod Grade

B.M. 323.37

↑ 5.7 328.00

Top 16" Pipe

Inlet 2.6.2 221.80 220.4

Top 16" Pipe

Outlet 9.7 218.30 216.9

146. 352.12

↑

NO pipe

153+99	36' - 12"		
	20' from @		
154	<u>356.97</u>		
X	1.00	<u>357.97</u>	
inlet	3.60	55.87	
I.S.	2.72	56.77	54.50 2.27
outlet	5.80	53.69	
O.S.	3.85	55.64	54.00 1.64
@ Road	3.00	56.49	

218+66

40' - 10" 22' to N. 18' to S.
 24' from @ on N.
 20' " " @ on S.

218	<u>302.61</u>		
X	4.12	<u>306.73</u>	
inlet	5.70	301.03	
I.S.	4.75	301.98	301.00 9.8
outlet	10.10	296.63	
O.S.	9.65	297.08	296.70 38
@ Road	4.10		

Sta.	Rad	Grade	
B.M		<u>361.27</u>	
X	0.6	<u>356.97</u>	
		<u>361.87</u>	
Top 10" Pipe In	5.9	355.97	354.89
12" " Ot.	7.3	354.57	353.49

218	4.0	302.61	
X	4.0	<u>306.61</u>	
Top 10" Pipe In.	5.1	301.50	300.6
10" " Ot.	9.79	296.90	296.0

223+29 30 - 10"
 20' from @

224	292.03		
π	5.52	297.55	
inlet	5.90	91.66	
I.S.	4.50	93.06	91.30 1.76
outlet	9.10	88.46	
O.S.	6.50	91.06	89.00 2.06
@ Road	4.10	93.46	

231+55 40 - 12"
 22' from @

232	239.93		
π	4.10	244.03	
inlet			
I.S.	0.52	43.50	41.80 1.70
outlet	good		
O.S.	3.07	40.96	40.00 9.6
@ Road	2.23	41.80	

Sta	Rod	Grade
B.M.		298.53
π	4.4	297.92
Top 10" Pipe In.	5.9	292.0
" 10" " Out.	8.2	289.70
		291.10
		298.80
232	239.93	239.93
π	6.82	246.75
Top 12" Pipe Inlet	4.34	424
" 12" " Outlet	5.95	40.85
		41.32
		39.78

235+92 40'-10"
 22 from @
 236 213.92
 T 3.47 217.41
 inlet —
 I.S. 0.90 16.51 12.50 4.01
 outlet good
 O.S. 3.30 14.11 12.00 2.11
 @ Road 2.90 14.51

245+26 42'-36"
 23' from @
 246 119.50
 T 13.02 123.52
 inlet 6.00 17.52 on rock
 I.S. 3.10 20.42 17.50 2.92
 outlet 9.90 13.62 on rock
 O.S. 7.34 14.18 13.00 .58
 Bridge
 floor 5.76 17.76

H.R. Richey 11. 21/31-06 culverts
 Livery 15.6 50
 1.50 50

Sta	Rod	Grade
236	213.92	
T	5.36	219.28
Top 10" Pipe Inlet	5.44	213.84
10" Outlet	6.31	212.97

246	119.50	
T	8.99	119.49
T.P.	5.75	113.74
Top 36" Pipe Outlet	2.87	116.62
T.P. T.P.	8.15	121.89
Top 36" Pipe Inlet	1.44	120.45



5/7, 07.

B.M. ¹¹⁷		301.05	
π	2.36	<u>303.41</u>	
115	3.07	300.34	300.75
116	3.51	299.90	299.50
117	4.61	298.30	298.25
118	6.81	296.60	297.00
119	8.71	294.90	299.00
T.P.	0.54	302.87	
π	12.90	<u>315.77</u>	
120	11.77	304.00	304.00
121	7.30	308.47	308.35
122	2.30	313.47	312.70
T.P.	1.21	314.54	
π	7.44	<u>322.00</u>	
123	4.94	317.06	317.05
124	3.35	318.65	318.50

5/28, '07

C.M.P.

B.M		323.37	
π	7.20	<u>330.57</u>	
135	3.07	327.50	327.50
134	5.37	325.20	325.00
133	4.77	325.80	326.00
B.M.	2.54	328.03	328.01
132	5.87	324.70	324.50
131	7.57	323.00	323.00
130	7.16	321.41	321.50
π	1.47	<u>322.88</u>	
129	2.98	319.90	320.00
127	4.73	318.15	318.42
126	4.48	318.40	318.34
125	4.58	318.30	318.25
124	4.28	318.60	318.50
123	6.07	316.81	317.05
π	0.33	<u>317.14</u>	
122	4.64	312.50	312.70
121	8.74	308.40	308.35
I.T.P.	12.66	304.48	
π	0.67	<u>305.15</u>	
120	1.53	302.62	303.50
119	5.78	299.27	299.00
118	8.05	297.10	297.10

on top grade stave

Finley Reames has 16'-10" iron pipe at field E. of garden.

5/28 07

X 305.15

117 6.25 298.90

298.25

116 5.15 300.00

299.50

115 4.25 300.90

300.75

Reset stakes 159 to to 172+36

Run a line straight between those

points 159 to 172 + 33 1/2

B.M.		<u>361.27</u>	
X	6.50	<u>368.07</u>	
153	9.30	358.97	359.25
152	7.80	<u>361.27</u>	360.50
151	5.97	362.10	361.75
150	5.97	362.10	363.00
149	7.47	360.60	362.00
148	9.67	358.40	359.00
147	12.53	358.54	356.00
X	2.54	<u>358.08</u>	
146	3.28	354.80	355.14
145	4.03	354.05	354.28
144	4.58	353.50	353.42
143	6.08	352.00	352.56
142	6.73	351.30	351.70
141	8.68	349.40	349.20
140	11.38	346.70	346.70
T.P. 7	12.21	345.87	
X	0.16	<u>346.03</u>	
139	4.06	341.97	342.00
138	7.93	338.10	338.10
137	12.00	334.13	334.00

Top grade stake

Changed Line.

June 18.

Ed Brundredge 1hr

						0	F.
BM	0.70			371.56			159+00 L N 86 $\frac{1}{4}$ W
159	372.26	3.85		3.15	368.41	369.00	.59
160		4.90		.95	367.46	368.05	.54
161		7.90		3.10	369.36	365.85	Telephone Pole 160+50
162		10.80		2.90	361.46	363.60	18 $\frac{1}{2}$ R of C.
163		9.80	1.00		362.46	363.90	.94
164		8.60	1.20		363.66	363.20	.46
TP	3.49	8.50	.10		363.76		163+40 Tel. Pole 22 $\frac{1}{2}$ R.
165	367.25	4.20		.71	363.05	363.09	.05
166		3.70	.50		363.55	363.00	.55
167		5.20		1.50	362.05	363.00	.95
168		5.90		.70	361.35	363.00	1.65
169		5.50	.40		361.75	363.70	1.95
170		4.10	1.40		363.15	364.40	1.25
171	7.80	3.52	.58		363.73	365.10	1.37
172	371.53	5.90	1.90		365.63	364.70	.93
+ 33 $\frac{1}{2}$		8.39		2.49	363.14		
173 old		13.00		4.61	358.53	362.10	3.97
	11.94	25.02	7.08	20.11	13.03		
		11.92		7.05			
		15.02		7.05			
				371.53			
169	6.68	9.80		368.41	361.73		
162	11.16	6.94		372.63	361.47		
		1.10			371.53		

Location Corner Stones.

June 26.07

85+61 Cottonwood N.W. 59'-10"
Sta 86 S.W. 49'-6" ✓

East ← Survey #9372.

30" Ash. W. 38'-3" ✓

- 40" Fence post N 25'-00"

Top Line S. Side Road.

or 105
Fence Post SW 18'-4"

" " SE. 19'-2"

N. Side Road. Do not move

24" Oak W 58'-1

197+92 E Post Fence 25'-4"

W " " 29'-1



		7/10, 27	
B.M. ¹⁵²		361.27	
Σ	2.02	363.29	
151	2.30	361.00	361.75
152	3.09	360.20	360.50
153	4.50	358.80	359.25
154	5.87	357.40	357.00
155	3.29	360.00	361.35
156	0.84	363.25	363.70
Σ	9.85	373.10	
157	7.00	366.10	366.05
158	5.10	368.00	368.40
159	4.60	368.50	369.00
160	5.00	368.10	368.00
161	7.30	365.80	365.80
162	9.40	363.70	363.60
163	9.80	363.30	363.40
164	7.50	363.60	363.20
165	7.70	363.40	363.00

No crown

Build Approach at school-house. Sta. 152.

Put in iron pipe.

Build approach at Reame's Tenant house.

Widen grade 129+50 to 131+30

" " 135

Smooth grade from Curls drive to school-house
also north slope

165-166 -) road on N. side
176+25 Big Swamp in N ditch
184-185 rough grade
185+22 187 N side High

E. M. Watkins wants culvert
near Sta. 109 located off wire
fence. He will cut outlet.

Side stake about 169 out of line
© " " 114 1' " " " "

111

111+50 cut 18' wide 18'

Ease grade 102 to 112

" " 595 to 77
284.00 297.00

" " 85 to 94

" " 72 to 80

" " 60 to 67 if possible



Grade sheet 52 to 54+55
54+55 ?

Ease grade 8 to 13
cut at least 2 feet deep
+ 2 cemetery gate 12+50
0 28.74

Sta. 1 to 7 Grade is above sidewalk
Sub grade could be 1.50' to 2.00' lower.

24
6
6
36

137 06
42-56
79 C 2