March 9 - 1904 -

On Wilfley West line measured from Big burr oak set stake at 5 ch. said by deed to be dist to sec <, fence and line at 54'

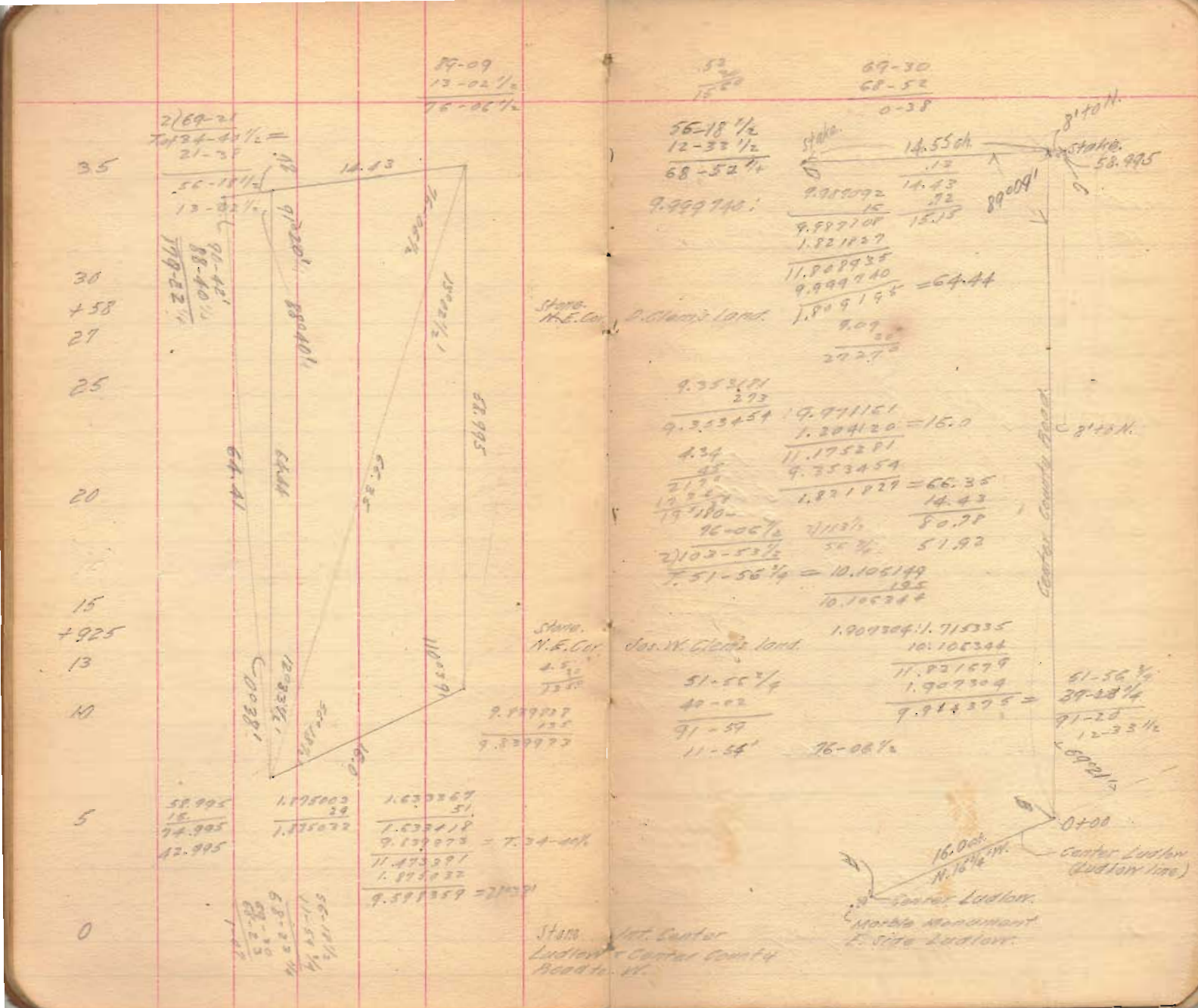
On S. line Sec. 4 - T. 3. R. 13 - from stone SW < Sec - large stone dug out from under 6" of dirt + on top 4" -

At 5.50 center Lees creek.
" 10+11 lks. line South
" - 20.22 " "
" 29.11 cor. post < Wyle which is 5.41 from oak (see opp. page)
At 40. set stake
" 40.40 center road
" 34.75 Lees Creek.
" 45.65 " "
" 57.60 old mill race
" 66.23 chris Mohr - Sam Hurst - on ~~South~~ north
" 72.75 Lees Creek
" 80.48½ Sec < stone.
Found this stone in prairie under 6" soil

On South line Sec 34 - T. 4. R. 13.
Measured East from Stone
SE Sec. 4 & SW Sec 34

at 19.70 Shenandoah Creek
" 40.53 fence line Ed Hurst &
Geo. Stutz north and Sam Hurst
& Faulkner south -
" 45.10 Graves creek
" 54.17 line on South - Faulkner
& Mary D. Adams
" 60.61 oak stump, supposed to
be witness tree -
" 69. Graves creek
" 73 " "
" set stake at 80.
" center pike from north
80.94

Measured from stone SW< Sec 3 -
North at 40.52 point claimed
for 1/4 <
Set stake at 80.00 and dug
for < at 81.04


89-09
13-02 1/2
76-06 1/2
69-30
68-52
0-38
56-18 1/2
12-33 1/2
68-52 1/4
stake.
14.55 ch.
stake.
58.995
8'+0 N.
89°09'
9.999948
9.999710
1.821127
11.820837
9.999710
1.820127
=64.44
State N.E. Cor.
J. Glenn's land.
9.353454
9.971151
1.381420
=16.0
11.352571
9.353454
1.821129
=66.35
14.43
80.78
51.92
96-06 1/2
2)102-53 1/2
51-56 1/4 = 10.105144
10.105144
1.907304
1.715335
10.105144
11.821679
1.907304
9.914375 =
Jos. W. Glenn's land.
51-56 1/4
40-02
91-58
11-54'
76-08 1/2
61-56 3/4
39-33 1/4
91-29
12-33 1/2
0+00
16.0 ch.
N. 16 1/2 W.
Center Ludlow
(Ludlow line)
Center Ludlow.
Marble Monument
E. side Ludlow.
Center County Road
8'+0 N.
2(69-21
Top 34-41 1/2 =
21-39
56-18 1/2
13-02 1/2
14.43
9°20'
64.44
58.995
64.44
14.55
11°45'
11°45'
11°45'

70
+.255
66
65

9.999968 : 9.999997 =
1.908539 = 81.01
1.908536
9.999968
1.908568 = 81.02

Stake.

60
+.995
58
55
50
45
40

Stake.

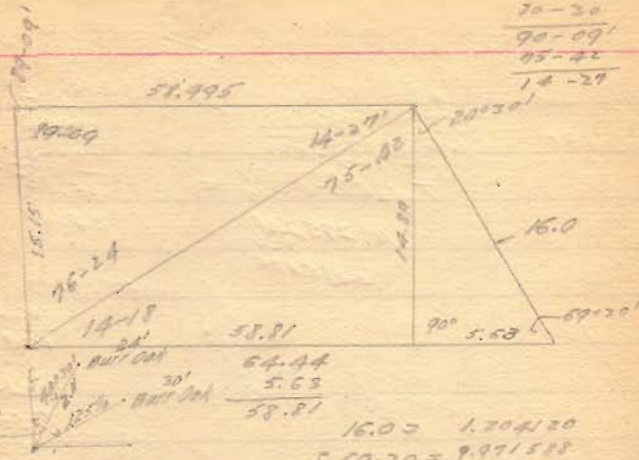
120-13
55-52½
176-05½
3-54½

8.836297 : 9.936598
0.805501
10.742079
8.836297
1.905782 =
80.50
.09
80.41

30.82
.30
924.60

8.834456 : 9.936578
0.805501
10.742079
8.834456
1.907623 =
80.84

8.832607
.925
8.833532 : 9.936578
0.805501
10.742079
8.833532
1.908547 = 81.01
.09
80.92




64.44
5.63
58.81

Set 8' to S. at this point.

16.0 = 1.204120
5.69-30 = 9.971588
1.175708 = 14.89

1.204120
9.544325 = 20-30
10.748445 = 5.63

1.175708 = 14.89
1.769451 = 58.81
9.406257 = 14-18

1.769451 = 58.81
9.986331 75.42
1.783120 = 60.69

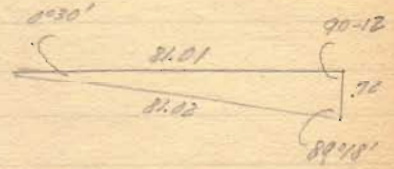
9.999952 : 9.397132
1.783120 = 60.69
11.180252
9.999952
1.180300 = 15.15
14.43
0.72

89-09
14-27
103-36
76-24
14-18
90-42

145.45
64.44
81.01

145.45
64.44
81.01

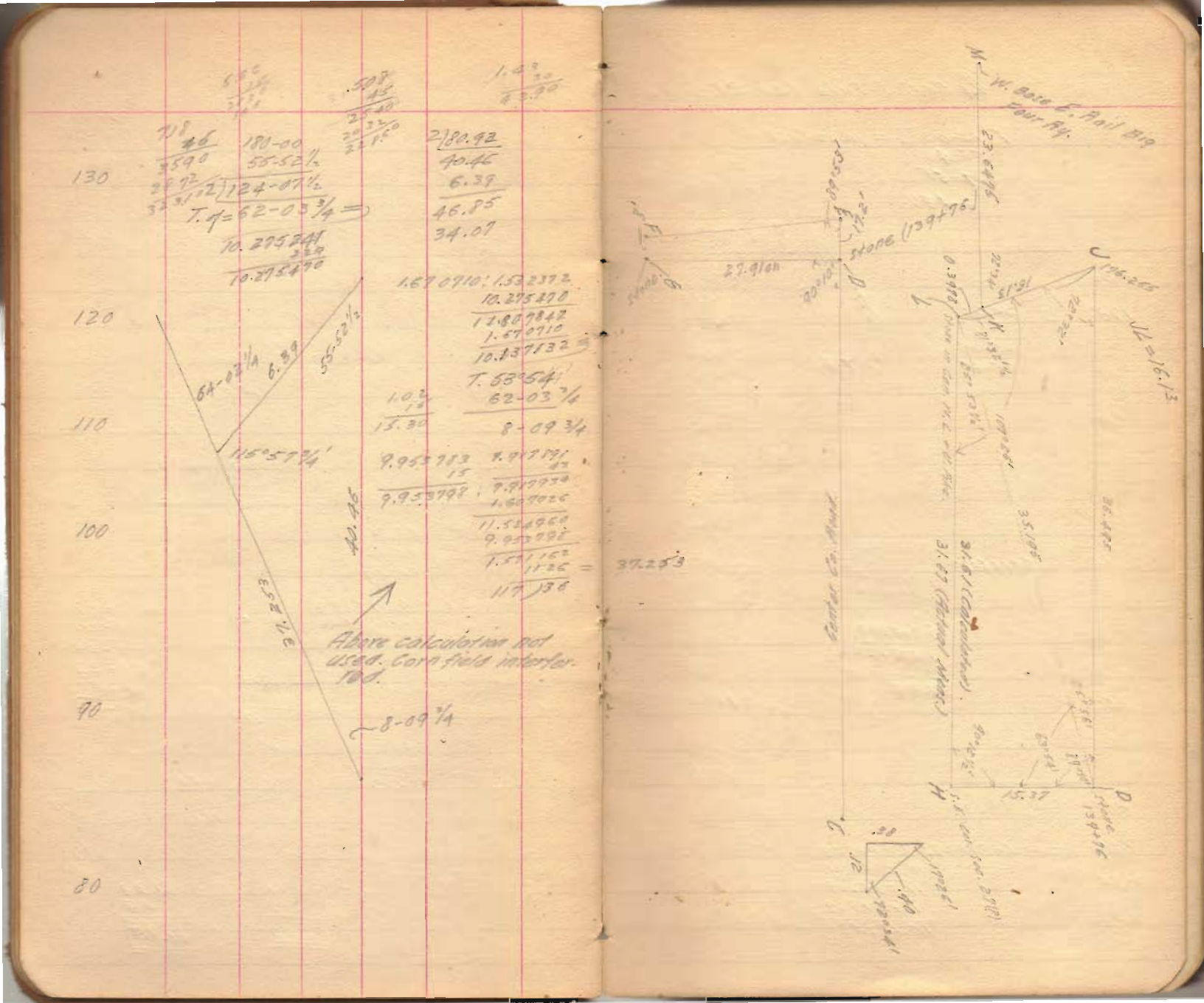
9.999968 : 9.940842
1.909770
9.850612
9.999968
.850644




64.44
.09
64.53

Stake

81.02
.09
81.93


W. Base E. Rail Brg
Four Brg.
Stone (139+96
Stone B
Stone C
Stone D
Stone E
Stone F
Stone G
Stone H
Stone I
Stone J
Stone K
Stone L
Stone M
Stone N
Stone O
Stone P
Stone Q
Stone R
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Stone T
Stone U
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Stone X
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Stone QQQQ
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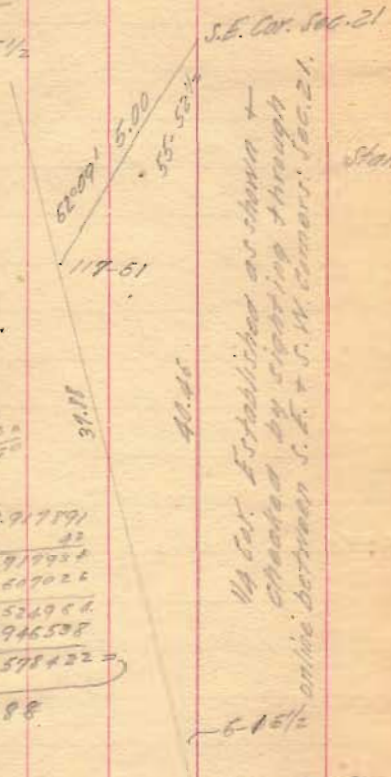
Stone SSSSSSSSSSSSSSSSSSSSSSSSS
Stone TTTTTTTTTTTTTTTTTTTTTTTTT
Stone UUUUUUUUUUUUUUUUUUUUUUUUU
Stone VVVVVVVVVVVVVVVVVVVVVVVVV
Stone WWWWWWWWWWWWWWWWWWWWWWWWW
Stone XXXXXXXXXXXXXXXXXXXXXXXXX
Stone YYYYYYYYYYYYYYYYYYYYYYYYY
Stone ZZZZZZZZZZZZZZZZZZZZZZZZZ
Stone AAAAAAAAAAAAAAAAAAAAAAAAAA
Stone BBBBBBBBBBBBBBBBBBBBBBBBBB
Stone CCCCCCCCCCCCCCCCCCCCCCCCCC
Stone DDDDDDDDDDDDDDDDDDDDDDDDDD
Stone EEEEEEEEEEEEEEEEEEEEEEEEEE
Stone FFFFFFFFFFFFFFFFFFFFFFFFFF
Stone GGGGGGGGGGGGGGGGGGGGGGGGGG
Stone HHHHHHHHHHHHHHHHHHHHHHHHHH
Stone IIIIIIIIIIIIIIIIIIIIIIIIII
Stone JJJJJJJJJJJJJJJJJJJJJJJJJJ
Stone KKKKKKKKKKKKKKKKKKKKKKKKKK
Stone LLLLLLLLLLLLLLLLLLLLLLLLLL
Stone MMMMMMMMMMMMMMMMMMMMMMMMMM
Stone NNNNNNNNNNNNNNNNNNNNNNNNNN
Stone OOOOOOOOOOOOOOOOOOOOOOOOOO
Stone PPPPPPPPPPPPPPPPPPPPPPPPPP
Stone QQQQQQQQQQQQQQQQQQQQQQQQQQ
Stone RRRRRRRRRRRRRRRRRRRRRRRRRR
Stone SSSSSSSSSSSSSSSSSSSSSSSSSS
Stone TTTTTTTTTTTTTTTTTTTTTTTTTT
Stone UUUUUUUUUUUUUUUUUUUUUUUUUU
Stone VVVVVVVVVVVVVVVVVVVVVVVVVV
Stone WWWWWWWWWWWWWWWWWWWWWWWWWW
Stone XXXXXXXXXXXXXXXXXXXXXXXXXX
Stone YYYYYYYYYYYYYYYYYYYYYYYYYY
Stone ZZZZZZZZZZZZZZZZZZZZZZZZZZ
Stone AAAAAAAAAAAAAAAAAAAAAAAAAAA
Stone BBBBBBBBBBBBBBBBBBBBBBBBBBB
Stone CCCCCCCCCCCCCCCCCCCCCCCCCCC
Stone DDDDDDDDDDDDDDDDDDDDDDDDDDD
Stone EEEEEEEEEEEEEEEEEEEEEEEEEEE
Stone FFFFFFFFFFFFFFFFFFFFFFFFFFF
Stone GGGGGGGGGGGGGGGGGGGGGGGGGGG
Stone HHHHHHHHHHHHHHHHHHHHHHHHHHH
Stone IIIIIIIIIIIIIIIIIIIIIIIIIII
Stone JJJJJJJJJJJJJJJJJJJJJJJJJJJ
Stone KKKKKKKKKKKKKKKKKKKKKKKKKKK
Stone LLLLLLLLLLLLLLLLLLLLLLLLLLL
Stone MMMMMMMMMMMMMMMMMMMMMMMMMMM
Stone NNNNNNNNNNNNNNNNNNNNNNNNNNN
Stone OOOOOOOOOOOOOOOOOOOOOOOOOOO
Stone PPPPPPPPPPPPPPPPPPPPPPPPPPP
Stone QQQQQQQQQQQQQQQQQQQQQQQQQQQ
Stone RRRRRRRRRRRRRRRRRRRRRRRRRRR
Stone SSSSSSSSSSSSSSSSSSSSSSSSSSS
Stone TTTTTTTTTTTTTTTTTTTTTTTTTTT
Stone UUUUUUUUUUUUUUUUUUUUUUUUUUU
Stone VVVVVVVVVVVVVVVVVVVVVVVVVVV
Stone WWWWWWWWWWWWWWWWWWWWWWWWWWW
Stone XXXXXXXXXXXXXXXXXXXXXXXXXXX
Stone YYYYYYYYYYYYYYYYYYYYYYYYYYY
Stone ZZZZZZZZZZZZZZZZZZZZZZZZZZZ
Stone AAAAAAAAAAAAAAAAAAAAAAAAAAAA
Stone BBBBBBBBBBBBBBBBBBBBBBBBBBBB
Stone CCCCCCCCCCCCCCCCCCCCCCCCCCCC
Stone DDDDDDDDDDDDDDDDDDDDDDDDDDDD
Stone EEEEEEEEEEEEEEEEEEEEEEEEEEEE
Stone FFFFFFFFFFFFFFFFFFFFFFFFFFFF
Stone GGGGGGGGGGGGGGGGGGGGGGGGGGGG
Stone HHHHHHHHHHHHHHHHHHHHHHHHHHHH
Stone IIIIIIIIIIIIIIIIIIIIIIIIIIII
Stone JJJJJJJJJJJJJJJJJJJJJJJJJJJJ
Stone KKKKKKKKKKKKKKKKKKKKKKKKKKKK
Stone LLLLLLLLLLLLLLLLLLLLLLLLLLLL
Stone MMMMMMMMMMMMMMMMMMMMMMMMMMMM
Stone NNNNNNNNNNNNNNNNNNNNNNNNNNNN
Stone OOOOOOOOOOOOOOOOOOOOOOOOOOOO
Stone PPPPPPPPPPPPPPPPPPPPPPPPPPPP
Stone QQQQQQQQQQQQQQQQQQQQQQQQQQQQ
Stone RRRRRRRRRRRRRRRRRRRRRRRRRRRR
Stone SSSSSSSSSSSSSSSSSSSSSSSSSSSS
Stone TTTTTTTTTTTTTTTTTTTTTTTTTTTT
Stone UUUUUUUUUUUUUUUUUUUUUUUUUUUU
Stone VVVVVVVVVVVVVVVVVVVVVVVVVVVV
Stone WWWWWWWWWWWWWWWWWWWWWWWWWWWW
Stone XXXXXXXXXXXXXXXXXXXXXXXXXXXX
Stone YYYYYYYYYYYYYYYYYYYYYYYYYYYY
Stone ZZZZZZZZZZZZZZZZZZZZZZZZZZZZ
Stone AAAAAAAAAAAAAAAAAAAAAAAAAAAAA
Stone BBBBBBBBBBBBBBBBBBBBBBBBBBBBB
Stone CCCCCCCCCCCCCCCCCCCCCCCCCCCCC
Stone DDDDDDDDDDDDDDDDDDDDDDDDDDDDD
Stone EEEEEEEEEEEEEEEEEEEEEEEEEEEEE
Stone FFFFFFFFFFFFFFFFFFFFFFFFFFFFF
Stone GGGGGGGGGGGGGGGGGGGGGGGGGGGGG
Stone HHHHHHHHHHHHHHHHHHHHHHHHHHHHH
Stone IIIIIIIIIIIIIIIIIIIIIIIIIIIII
Stone JJJJJJJJJJJJJJJJJJJJJJJJJJJJJ
Stone KKKKKKKKKKKKKKKKKKKKKKKKKKKKK
Stone LLLLLLLLLLLLLLLLLLLLLLLLLLLLL
Stone MMMMMMMMMMMMMMMMMMMMMMMMMMMMM
Stone NNNNNNNNNNNNNNNNNNNNNNNNNNNNN
Stone OOOOOOOOOOOOOOOOOOOOOOOOOOOOO
Stone PPPPPPPPPPPPPPPPPPPPPPPPPPPPP
Stone QQQQQQQQQQQQQQQQQQQQQQQQQQQQQ
Stone RRRRRRRRRRRRRRRRRRRRRRRRRRRRR
Stone SSSSSSSSSSSSSSSSSSSSSSSSSSSSS
Stone TTTTTTTTTTTTTTTTTTTTTTTTTTTTT
Stone UUUUUUUUUUUUUUUUUUUUUUUUUUUUU
Stone VVVVVVVVVVVVVVVVVVVVVVVVVVVVV
Stone WWWWWWWWWWWWWWWWWWWWWWWWWWWWW
Stone XXXXXXXXXXXXXXXXXXXXXXXXXXXXX
Stone YYYYYYYYYYYYYYYYYYYYYYYYYYYYY
Stone ZZZZZZZZZZZZZZZZZZZZZZZZZZZZZ
Stone AAAAAAAAAAAAAAAAAAAAAAAAAAAAAA
Stone BBBBBBBBBBBBBBBBBBBBBBBBBBBBBB
Stone CCCCCCCCCCCCCCCCCCCCCCCCCCCCCC
Stone DDDDDDDDDDDDDDDDDDDDDDDDDDDDDD
Stone EEEEEEEEEEEEEEEEEEEEEEEEEEEEEE
Stone FFFFFFFFFFFFFFFFFFFFFFFFFFFFFF
Stone GGGGGGGGGGGGGGGGGGGGGGGGGGGGGG
Stone HHHHHHHHHHHHHHHHHHHHHHHHHHHHHH
Stone IIIIIIIIIIIIIIIIIIIIIIIIIIIIII
Stone JJJJJJJJJJJJJJJJJJJJJJJJJJJJJJ
Stone KKKKKKKKKKKKKKKKKKKKKKKKKKKKKK
Stone LLLLLLLLLLLLLLLLLLLLLLLLLLLLLL
Stone MMMMMMMMMMMMMMMMMMMMMMMMMMMMMM
Stone NNNNNNNNNNNNNNNNNNNNNNNNNNNNNN
Stone OOOOOOOOOOOOOOOOOOOOOOOOOOOOOO
Stone PPPPPPPPPPPPPPPPPPPPPPPPPPPPPP
Stone QQQQQQQQQQQQQQQQQQQQQQQQQQQQQQ
Stone RRRRRRRRRRRRRRRRRRRRRRRRRRRRRR
Stone SSSSSSSSSSSSSSSSSSSSSSSSSSSSSS
Stone TTTTTTTTTTTTTTTTTTTTTTTTTTTTTT
Stone UUUUUUUUUUUUUUUUUUUUUUUUUUUUUU
Stone VVVVVVVVVVVVVVVVVVVVVVVVVVVVVV
Stone WWWWWWWWWWWWWWWWWWWWWWWWWWWWWW
Stone XXXXXXXXXXXXXXXXXXXXXXXXXXXXXX
Stone YYYYYYYYYYYYYYYYYYYYYYYYYYYYYY
Stone ZZZZZZZZZZZZZZZZZZZZZZZZZZZZZZ
Stone AAAAAAAAAAAAAAAAAAAAAAAAAAAAAAA
Stone BBBBBBBBBBBBBBBBBBBBBBBBBBBBBBB
Stone CCCCCCCCCCCCCCCCCCCCCCCCCCCCCCC
Stone DDDDDDDDDDDDDDDDDDDDDDDDDDDDDDD
Stone EEEEEEEEEEEEEEEEEEEEEEEEEEEEEEE
Stone FFFFFFFFFFFFFFFFFFFFFFFFFFFFFFF
Stone GGGGGGGGGGGGGGGGGGGGGGGGGGGGGGG
Stone HHHHHHHHHHHHHHHHHHHHHHHHHHHHHHH
Stone IIIIIIIIIIIIIIIIIIIIIIIIIIIIIII
Stone JJJJJJJJJJJJJJJJJJJJJJJJJJJJJJJ
Stone KKKKKKKKKKKKKKKKKKKKKKKKKKKKKKK
Stone LLLLLLLLLLLLLLLLLLLLLLLLLLLLLLL
Stone MMMMMMMMMMMMMMMMMMMMMMMMMMMMMMM
Stone NNNNNNNNNNNNNNNNNNNNNNNNNNNNNNN
Stone OOOOOOOOOOOOOOOOOOOOOOOOOOOOOOO
Stone PPPPPPPPPPPPPPPPPPPPPPPPPPPPPPP
Stone QQQQQQQQQQQQQQQQQQQQQQQQQQQQQQQ
Stone RRRRRRRRRRRRRRRRRRRRRRRR

1/4 Cor. S. Side Sec. 21-5-13

T. 62-03 3/4 = 10.275470
55-47 1/4
117-51
6-16 1/2




+25.5 Stake W.L. + Urbana Pike. (near W. side)

176 40.46
5.00
45.46
35.46

170

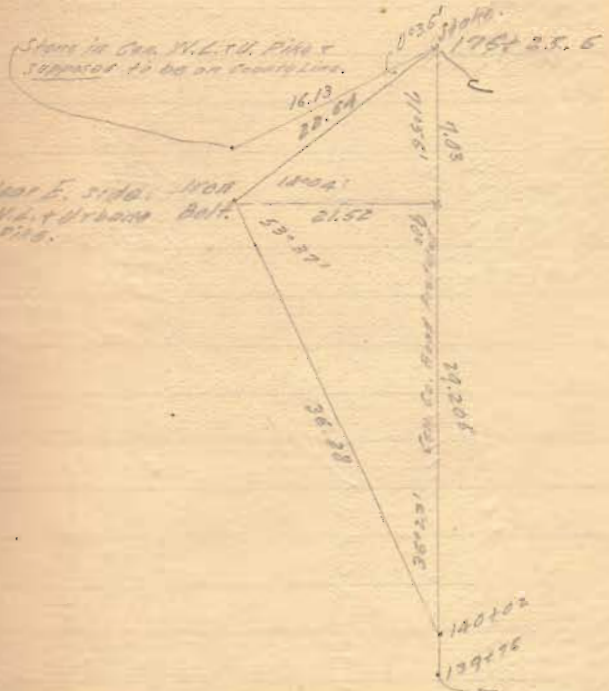
1.43
30
1.29

160 9.946538 9.917891
42
9.917934
1.607026
11.524964
9.946538
1.578422 =
37.88

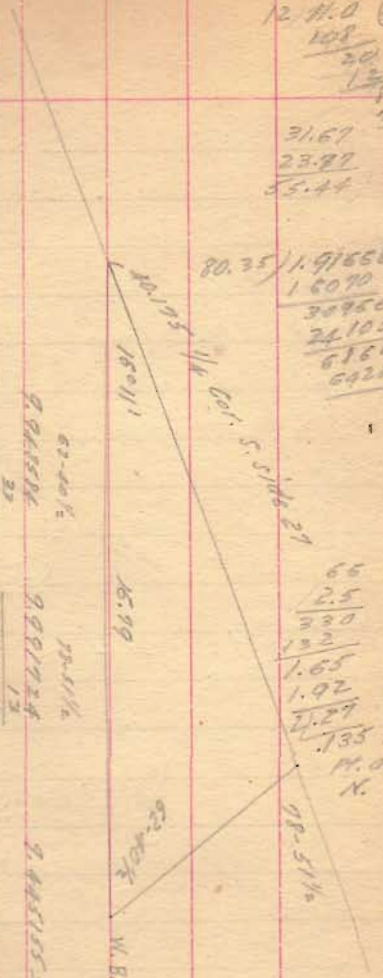
150

+02 L. 36°23'

140 1.657629: 1.549739 4.53
10.275470
+76 11.825209 Stone.
139 1.657629
10.167580 = 55-47 1/4
7475
4.53) 105.0 (23
90.6
1440




W. side Sec. 21 S. 27.91 ch. to stone S.W. > Warge's land. Set stake 15.41 ch. S. of stone.




12 11.0 (916
108
20
12
80
72
80

31.67
23.87
55.44

80.35 ) 1.916666 (.0213
16070
30966
24105
68660
64280

66
2.5
330
132
1.65
1.92
2.27
.135 More old Pt. at 1/4 Cor. N.

1.09
30
32.70
.42
30
12.60

9.991734 9.948617
1.225051
11.173665
9.991737
1.181929 = 15.20
8.505
23.705

9.948584
23
9.948617
1.225051
11.173668
9.446155
1.928513 =
5.352

62-40½
78-51½

9.991724
13
9.991737
1.225051
11.216788
9.948584
1.268204 =
18.54
8.505
12
27.175

9.445155 = 16-11

9.991734 : 9.445155
1.225051
10.670206
9.991734
0.678469 = 4.769

23.6475
12
23.7675

80.35 ) .27000 .00336
24105
28950
24105
48450

55.44
.00336
33264
16632
16632
.1862784 =
More old Pt. on Ry. N.

55.44
.0238
44352
16632
11088
1.319472

82 ) 1.916
.958

2 ) 23
11½

1.32
12
2.64
132
15.84

58.995
16
74.995
42.995

2)69-21
T. of 34-40½ = 9.839838
135
9.839973

4.5
30
135

1.875003
29
1.875032

1.633367
52
1.633419
9.839973
11.473392
1.875032
9.598360 =
T. of 21.38

9.09
30
272.70

34-40½
21-38
13-02½
56-18½

89-09
13-02½
76-06½

4.34
45
2170
1736
195.30

9.353181
273
9.353454

9.071161
1.204120 = 16.0
11.195281
9.353454
1.821827 =

2)118½
56¾
180
76-06½
2)103-53½
51-56¾ =

66.35
16.15
81.50
51.20

10.106149
195
10.106344

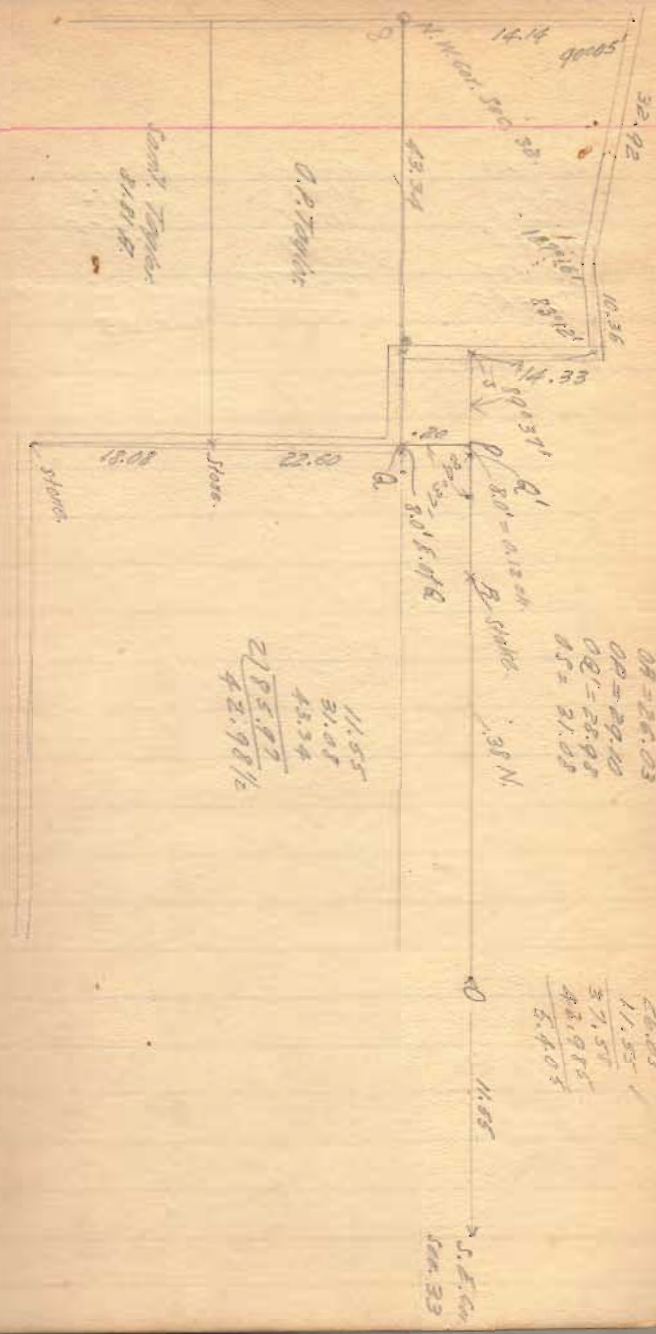
1.911158: 1.709270
10.106344
11.815614
1.911158
T. 9.904456

38-45¼
51-56¾
90-42
13-11½

.52
30
15.60

9.999968:

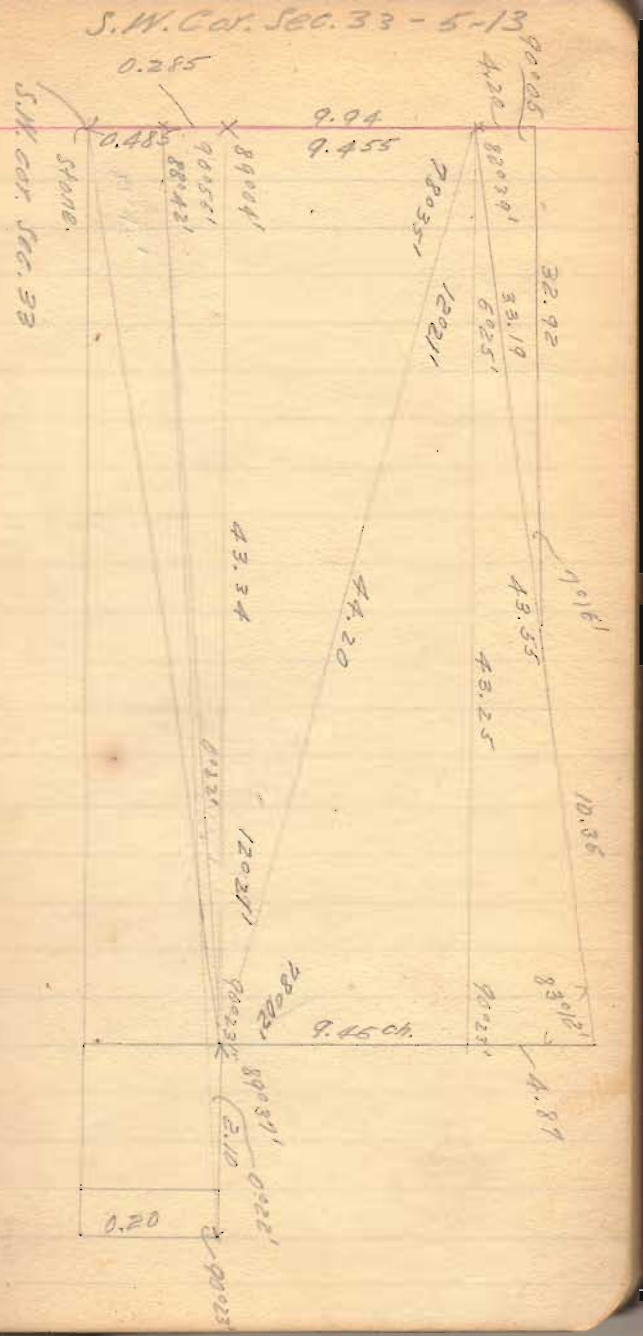
9.987092
16
9.987108
1.821841 = 66.35
11.808949
9.999968
1.808981 =
64.41



43.34
2.10
.21
45.65
42.985
2.665

43.34
31.08
11.55
2 | 85.97
42.985

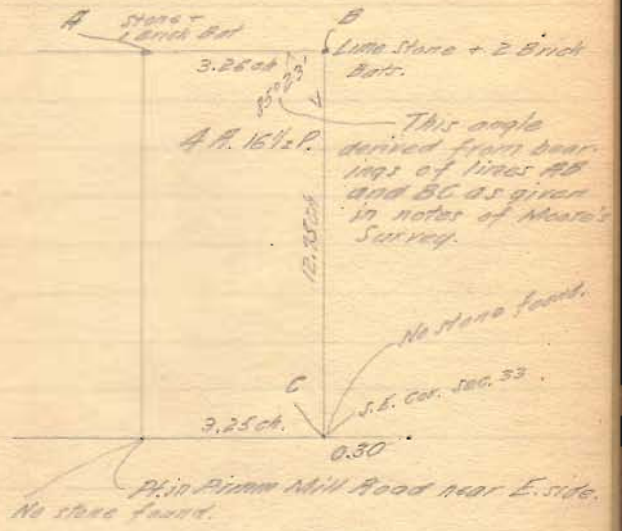
43.34
42.985
0.355
1/4 Cor. S. side Sec. 33.

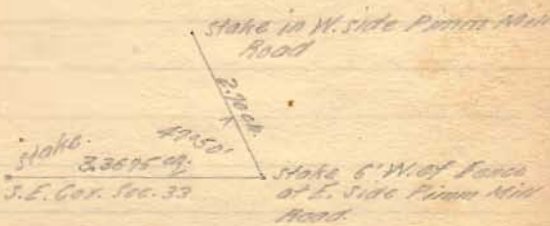


S.E. Cor. Sec. 33-5-13

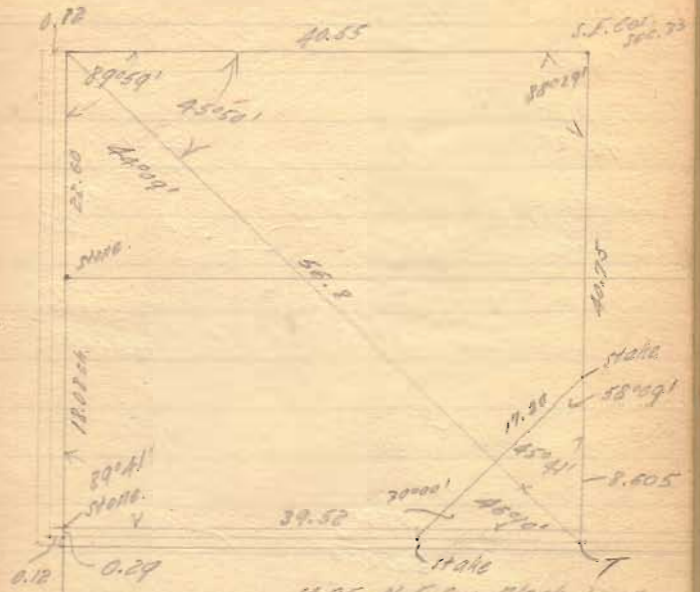
Notes of Survey By H.C. Moore in 1859.

Found Corners A & B and established S.E. cor Sec. 33 from same in manner shown below.




Located S.E. Cor. Sec. 33 from Moore's Survey.

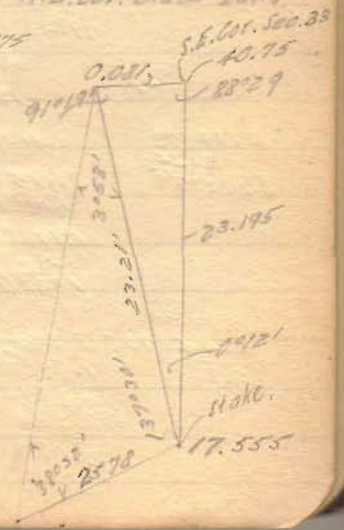



14.95 N.E. Cor. Block Land

18.08
22.60
.29
40.97

24.8975

40.75
17.555
23.195




8.95
.64
8.605
18.195 N. from T. to
S. line Scott's land.

18.195
4
72.780

209.81
15
1049.05
2098.1
3147.15

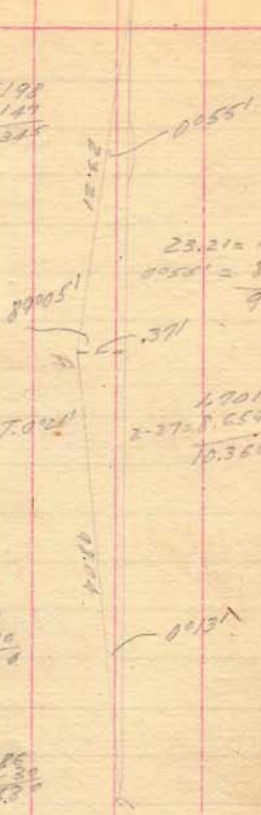
2)1-08½
T. of 0-34¼ = 7.995198
+ 3147
= 7.998345

98.04
23.21
121.25
74.83

2.083503
179
2.083682 : 1.874076
7.998345
9.872421
2.083682
7.788739 = T. 0°21'

23.21 = 1.365675
0°55' = 8.204070
9.569745 =
.371

1.701395
2-37 = 8.659475
10.360870 = 2.295



107.21
30
3216.30

80.86
30
2425.80

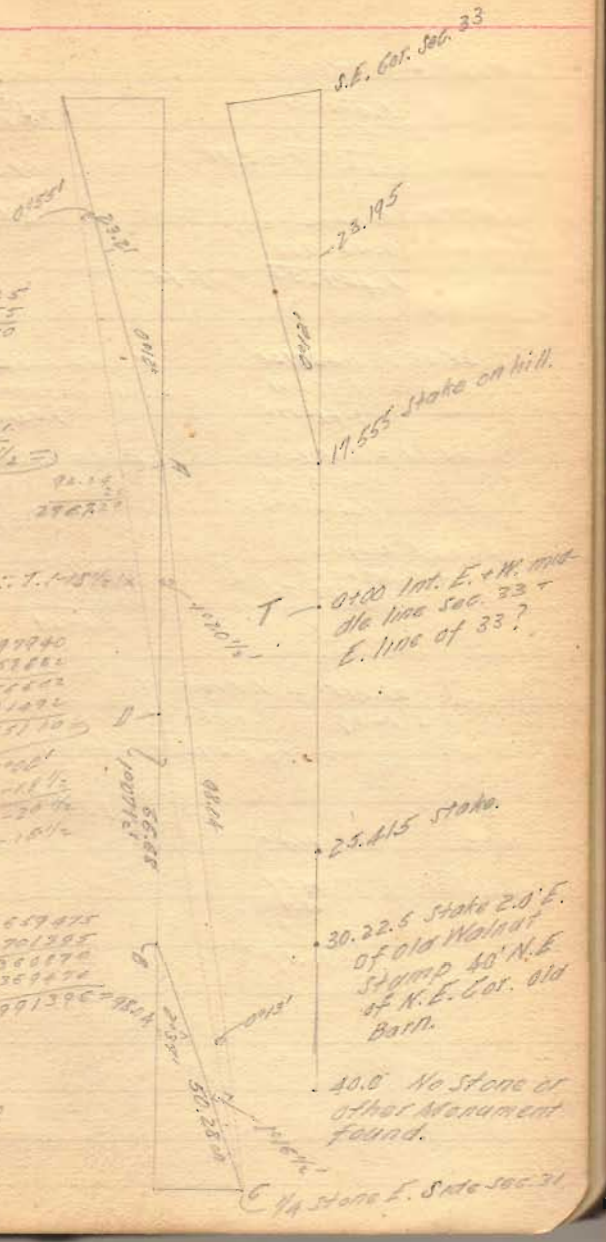
8.289773
3126
8.293899

8.413068
2426
8.415494
1.701396 = 50.28
10.116889
8.292899
1.823990 = 66.68

30.225
17.555
AB = 47.780
66.68
18.90

8.204070 : 8.296207
1.991396 = 98.04
10.287603
8.204070
2.083533 =
07
30 = 121.21

179°48'
1-20½
181-08½




AB = 30.225
17.555
47.780
BC = 50.28
98.06
2.50

2)2°37'
T. of 1-18½ =
8.355895
2767
8.358662

98.06 : 2.50 :: T. 1-18½

1.991492 : 0.397940
9.358662
8.756602
1.991492
6.965110 =

0°02'
1-18½
1-20½
1-16½

89.9
269.70

8.366777
2697
8.369474 : 8.659475
1.701395
10.360870
8.369474
1.991396 = 98.04

23.20
17.555
30.225
50.28
121.260

10.135 = 1.005609
214
1.005823
T.15-30 = 9.442988
10.408811 = 2.81

8.17 = 0.912222
T.15-30 = 9.442988
1.469234 = 29.46

26.86 = 1.429106
S. 74-30 = 9.983911
1.445195

29.46 = 1.469233
9.983911
1.485322

2.60 = 0.414973
S. 17-09 = 9.469637
9.884610 = .7668

38.075 = 1.580583
S. 1-39 = 8.459301
10.039884 = 1.099
.767
1.866

78.93

81.66
1.75
79.91
78.93
.98
80.89

10.98
2.81
8.17

29.46
26.86
2.60

90
17-09
72-51

10.135 = 1.005609
S. 74-30 = 9.983911
1.021698

2.60 = 0.414973
S. 72-51 = 9.980247
0.395220 = 2.485

17-09
15-30
1-39

38.075
2.485
40.560

42.08
1.75
40.33

30.57
2.485
28.085

80.66
42.08
38.58

80.89
42.08
38.61
40.56
1.95

30.57
10.52
3.475
44.565
82.64
38.075
28.00
18.075
2.485
20.560

30.57
10.52
41.09
3.475
44.565
2.485
42.080
82.64
40.56

3.475
10.52
28.085
42.080
82.64
40.560

82.64
1.76
80.88

| | | | | |
|---|---|---|---|---|
| 81.91 | | Stone N.W. Cor. 38 | 0.33 | E. of line. |
| 80. | | | | |
| 70 | | | | |
| 61.85 | | | | |
| 60 | | Line Hartzler + | Kirkwood. | |
| 51.12 | | | | |
| 50 | | | | |
| | | Line Kirkwood hrs. | + Wm. Kirkwood. | |
| 40.885 | | ½ Stone 0.30 E. line. | | Center of E. + W. Road. |
| 30 | | | | |
| 20 | | | | |
| 17.04 | | Center Pike. | | |
| 16.74 | | S. side Pike | | |
| 10 | | | | |
| 0 | N. 4½° E | Stone S.W. Cor. Sec. 38 | | + 0.30 ch. E. of line |

66.6
107.4
4)174.0
43.5
40.50
84.00

40.885
41.005
81.890
.02
81.91

81.15 1/3 Spike in Road

81.13 Stone 0.16 N. of Line. (Cor. 4-10-9-3)

80

81.13
40.55
40.58

0.16 = −1.204120
40.58 = 1.608312
7.595808 = 0° 14'

48.83
40.55
8.28

81.13
40.55
40.58 ) .16000 ( .0394
12174
38260
36522
17380

.00294
8.28
3152
788
3152
.0325232 Cor. at 48.83

70

40.58

60

50 Bolt in Road.

48.83 Stone

40.55 Tp. Line. D.R. 0°14' Center Road. 0.35' N. of line. Corrected line and ran West.

40

30

40.55 ) .35000 ( .0086
32440
25600
24330

20

17.75
.0086
10650
14200
.152650

10

0 N. 86° W. Stone at S.E. Cor. Sec. 4

0.2375 = -1.375664
38.67 = 1.587374
.788290 = 0°21'

80

77.295 75.45 / 38.625 / 36.825 — 77.50 / 2.05 / 75.45 / 1.84½ / 77.295 / 38.625 / 38.670 — Stone. 0.2375 N. of Line. Corrected line and ran W. with D.A. 1°04'
S.W. Cor. 10

70

60 — 0.23750 .00614 / 23202 / 5480 / 3867 / 16130

36.825 / .00614 / 147300 / 36825 / 220950 / .22610550

50 — .2375 / 2 / 7)4750 / 3 / 7)14250 / 20.3

40

38.62½ Corrected line + ran W. Stone. 0.03 N. of Line. D.A. 0°21'

30

29.10 Nail. Opp. old Stump on Left.

20

19.35 Stake

10

0 Stone S.E. Cor. Sec. 10

83.15 .305 S. of Cor. Corrected line + ran W. — Nail on Bridge. S.E. Cor. 22 + S.W. Cor. 16

83.08 — Nail on Bridge.

83.00 — Stake N. of E. end of Bridge.

80

74.0325 — Nail.

70

64.085 — 83.00 / 8.9675 / 74.0325 — Nail. Land Line Core + Clam.

62.38

60

50

41.56 ) .04500 .00108
4156
34400

41.56 D.L. 0°55' + 0°26 / 1°21' — .045 / 2 / .09 / 3 / 7)27 / 4 — Stake.

18.06
.00108
14448
1806
.0195048

40

30

20.77 — Stone — Nail Land Line

20

18.06 — Nail.

10

0 — D.R. 1°04' − 0°4' = 1°00' — Stone S.W. Cor Sec. 10 + S.E. Cor. 16

14.94 N. to N.E. Cor. Wren.
12.22 S. to Cor.
40.11 S. to 1/4 Cor.

9.425530 : 9.858877
0.919340 = 8.305
10.778217
9.425530
1.352687 = 22.525
41.56
64.085
62.33
1.755

41.56
20.77
62.33

64.085
1.705
63.380

S. to 1/4 Cor. 80.60 Corrected line + ran W.

74.0325
41.56
32.47

83.15
41.56
41.59

41.59 ) 30.500 .00733
29113
13870
12477
13930

32.47
.00733
9741
9741
22729
.238025 Cor. for 32.47

.305
2
.610
3
7)1830
26

.305 = 1.484300
41.59 = 1.618989
.865311 = 0°25'

64.085
41.56
22.525
.00733
67575
67575
157675
16.510825

| | | | |
|---|---|---|---|
| 82.10 | 12¼ / 3 / 7)36¾ / 5 | | Stake. |
| 80 | | | |
| 76.44 | | | Nail in Carlisle Pike. |
| 70 | | | |
| 65.22 | 2)82.10 / 41.05 / 40. / 1.05 | | Nail Stone 0.05 |
| 60 | | | |
| 58.84 | | | Nail. |
| 50 | .1225 / 41.05 / 6125 / 1225 / 4900 / 5.028625 / 4926 / 1026 / 821 / 3652 | 2).1225 / .0612 / .0612 | |
| 41.05 | | | Stake ¼ Cor. |
| 40 | 821 | | Stake. |
| 30 | | | |
| 22.93 | | | Nail |
| 20.27 | | | Nail |
| 20 | | | |
| 10 | | | |
| 0 | D.A. 0°10' − 0°05' = 0°05' | | S.E. Cor. Sec. 22 + S.W. Cor. 16 |

0.12¼ S. of line.

9.978083 : 9.985480
0.833147
10.818627
9.978083
0.840544 =
6.929

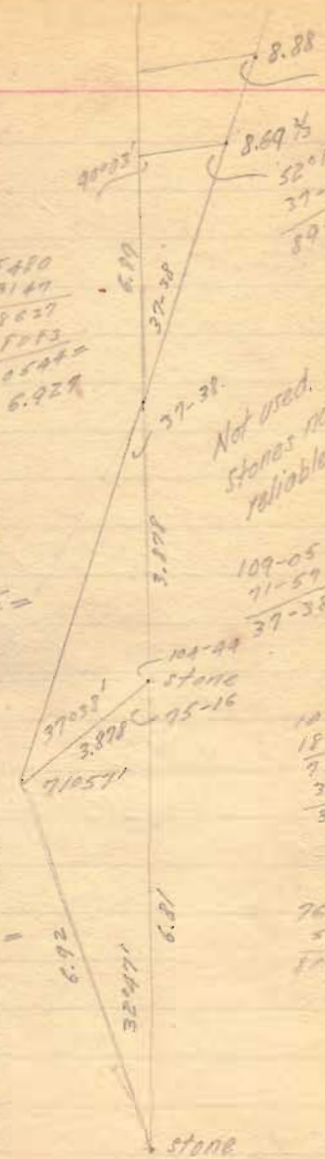
S. of line.

9.785761 : 9.985480
0.588633
10.574113
9.785761
0.788352 =
6.143

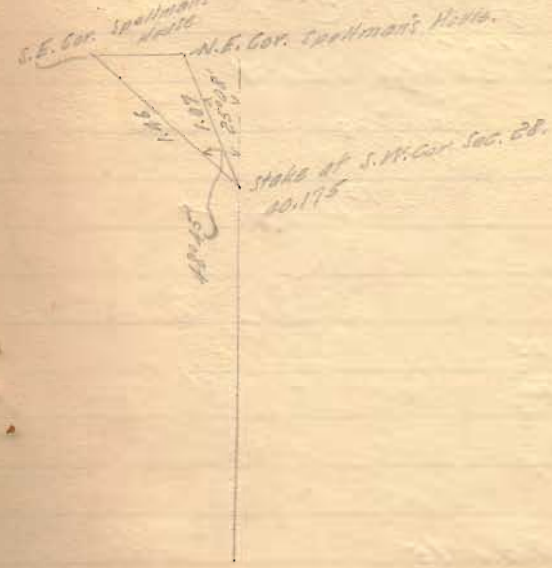
9.978083 : 9.933569
0.833147
10.566716
9.978083
0.588633 =
3.878

0.939519
9.785761
0.725280 = 5.31

0.939519
9.898494
0.838013 = 6.89
3.88
10.77



| | | | | | | |
|---|---|---|---|---|---|---|
| 40.19 | | | | | Stake | 0.72 N. of line. |
| 40 | | | | | | |
| | | 0.72 = | −1.857332 | | | |
| | | 40.19 = | 1.604118 | | | |
| | | | .253212 | | | |
| 30 | | | | | | |
| 20.095 | | | | | Center Road. | |
| 20 | | | | | | |
| 10 | | | | | | |
| 0 | Ran E. D.L. 1°02' | | | | 1/4 Stone S. line 28 | |
| 40.175 | | | | | Stake S.W. Cor. Sec. 28 | 0.05 N. of line. 40.46 1/2 N. to 1/4 Stone. |
| 40 | | | | | Nail. | |
| | 40 : 22.2 | | | | | |
| | .05 | | | | | |
| | 40 ) 1.110 ( .0277 = .02 3/4 Cor. for 22.2 | | | | | |
| 30 | 80 | | | | | |
| | 310 | | | | | |
| | 280 | | | | | |
| | 300 | | | | | |
| 22.20 | | | | | Nail. | |
| 20 | | | | | | |
| 10 | | | | | | |
| 4.25 | | | | | Cor. Road to South. | |
| 0 | Ran W. | | | | 1/4 Stone S. line 28 | |



80.71 2/3

Stone. 0.87½ N. of line.

80

66.01
.44
26404

80.72
40.25
40.47

0.87 1/3
3
29.0444
24216
48284
41432

80.72
.36

70

7)262
37

66.01
40.25
25.76

66.01

Stake. Set 0.516 S. of line.

60

25.76
43.3
7728
7728
10304
11.15408
8094
30600
28329
12718

(.27)

80.72: 66.01
.873
19803
46207
52808
57.62673 (.713

50

40.25

80.72) 57.62673
56504
71227
80 72
31558

D.B. 0°37'

40

1/4 Set Stake. 0.516 S. of line

.873
40
34.920 (.4326

80.72)
32288
26320
24216
21040
16144
48960

30

26.65

Land line. Adams & Taylor

20

.22
2
44
3
7)132
16

19.25
22
3850
3850
4.2350
4025
21000

.406

10

0

D.B. 0°16'

S.W. Cor. Sec. 28

90
5.23
84-37

50.06

5.503

5.429

44.63

91-33
66-28
158-01
21-59

8.972289
0.740600
9.712889 = 0.5163

18.26
12.757
5.503

.713
.077
.636

80.72
66.01
14.71
.213
4413
14.71
39.42
3.13325
28.329

(.077

9.572323 : 9.962288
0.894482 = 7.843
10.856770
9.572323
1.284447 = 19.25

.273
36
.634

40.47)
106531
100
106701
30033

0.740600
9.998080
0.738680 = 5.479

8.972289 : 9.126126
1.106701 = 12.785
10.232826
8.972289
1.261537 = 18.26
01
36

19.25

30.81
5.48
25.33
19.25
44.58
40
4.58

8.972289 : 9.354271
1.106701
10.460972
8.972289
1.488683 = 30.81
19.25
50.06

.873
44
43.3
.212
.221

13-04
5-23
7-41

43.3
2
.866
3
7)2598
37

91°33'

7.843

0100

88°27'

80

70

60

50

40

30

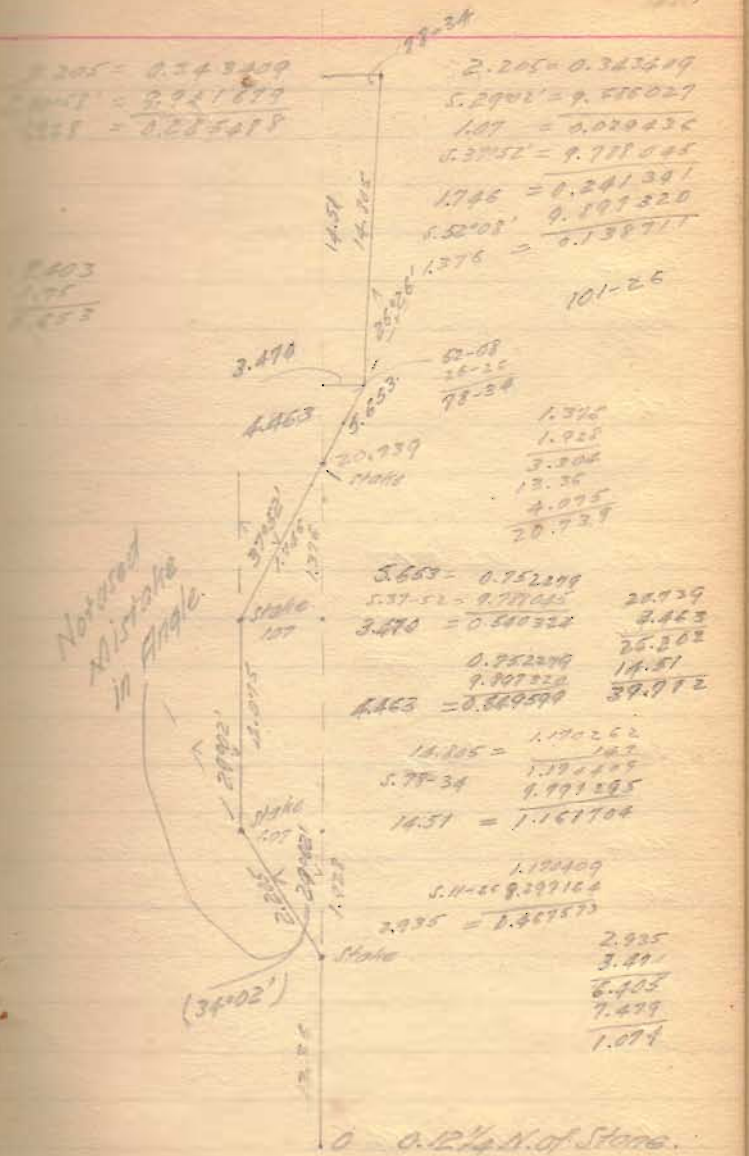
20

10

0.

Not used. Error in Angle.

Stone S.W. Cor. Sec. 34



80.887
80

Stone
S.W. Cor. Sec 4
1.032 N. of Stone

70

63.693

60

54.924

Stake 0.54 N. of Fence

50

40.15 D.L. 0°17'

Stake S. to Cen. Road 40.04 (E. & W. Road)
N. to Cen. Road to E. 36.195

40

.873
.123
.750
3
150
3
7)450
64

30

21.692
.75
108460
151844
40.15) 16.26900
16060
20900

21.692

Stake
.405
.123
.528 Cor. for 21.692

20

13.345
.75
66725
93416
40.15) 10.00875
8030
19787
16060
3727

Stake
.249
.123
.372 Cor. for 13.345

13.345

10

0 D.L. 1°04'

S.W. Cor.
Sec. 34

2.205 = 0.343409
S.34-02 = 9.747936
1.234 = 0.091345

4.075 = 0.610128
S.85-00 = 9.998344
= 0.608472

55-58
29-02
85-00
37-52
122-52
180
57-08

7.403
2.928
4.475

26-26
57-08
83-34

2.928
1.75
1.178

.90
.542
.351

2.205 = 0.343409
S. 55°58' = 9.918404
4.087 1.827 = 0.261813

4.075 = 0.610128
S.5°00' = 8.940296
0.355 — 1.550424
1.234
1.589 = 0.201124
S.32-52 = 9.734549
2.928 = 0.466575
S.57-08 9.924246
2.46 = 0.390821

26-26
57-08
96-26
180-00

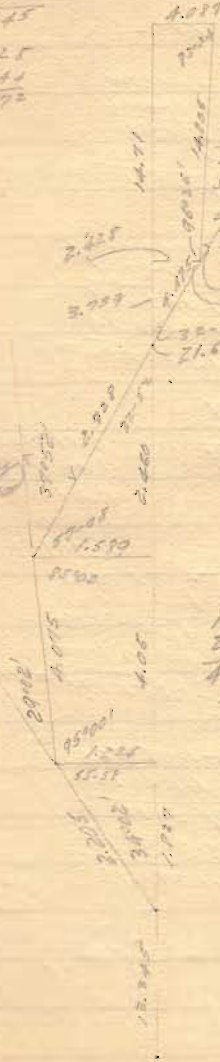
4.475 = 0.650793
32-52 = 9.734549
2.428 = 0.385342

4.475 = 0.650793
57-08 = 9.924246
3.759 = 0.575037

14.805 = 1.170409
6-26 9.049400
1.659 = 0.219809
2.428
4.087

14.805 = 1.170409
83-34 = 9.997259
14.71 = 1.167656

13.345
1.827
4.06
19.232
2.460
21.692
3.759
14.71
40.151



80.887 : 63.693 :: 1.032 : X

907841
38
907879

0.013700
1.804091
1.817791
80.87 = 1.907879
-1.909912 = .8127 Cor. for 63.693

4.087
.7007
.1225
4.9102
4.627
.2832

0.013700
1.739731
1.753431
1.907879
-1.845552 = .7007 Cor. for 54.924

.1225
.8233
54
2832

1.032
.123
.909

4.087
54
4.627

0.013700
1.603686
1.617386
1.907879
-1.709507

.909 = -1.958564
1.804091
1.762655
1.907879
-1.854776 = .7158
.123
.8388 Cor. for 63.693

Based on st. line between sec. corners.

-1.958564
1.739731
1.698295
1.907879
-1.790416 = .6172
.123
.7402 Cor. for 54.924

23.54
.19½
21186
2354
1177
40.74) 4.5903 (.112
4.074 .837
5163 .949
4074 4.087
1089 5.036
Cor. for 63.69

89-36
17
89-19

54.92
40.15
14.77

63.69
40.15
23.54

4.087 = 0.611405
16-52 = 9.462616
14.08 = 1.148789

14.08 = 1.148789
73-68 = 9.980904
13.79 = 1.129693

3.557 = 0.551084
16-52 = 9.462616
1.032 = 0.013700

3.557 = 0.551084
73-08 = 9.980904
3.404 = 0.531988

80.887
40.15
40.737

4.087
1.032
5.119
4.924
.195
2
.390
2
7 11.7
17

14.77
.19½
13293
1477
738
40.74) 28801 (.0706
28518
283.00

.0706
.837
.9076 Cor. for 54.92
4.087
4.9946
4.627
.3676

80.097 — Stone S.W. Cor. Sec. 10

80

80.10
39.92
40.18

70

39.92
18.425
21.495
.37
150465
64485
8.03315
39.92
4915

60

(.201
.13

56.82 — 39.92 — Land Line.

50

40

1/4 Cor.

39.92 — Nail in Floor of Bridge. 1/4 Cor. Set 0.13 N. of line

30

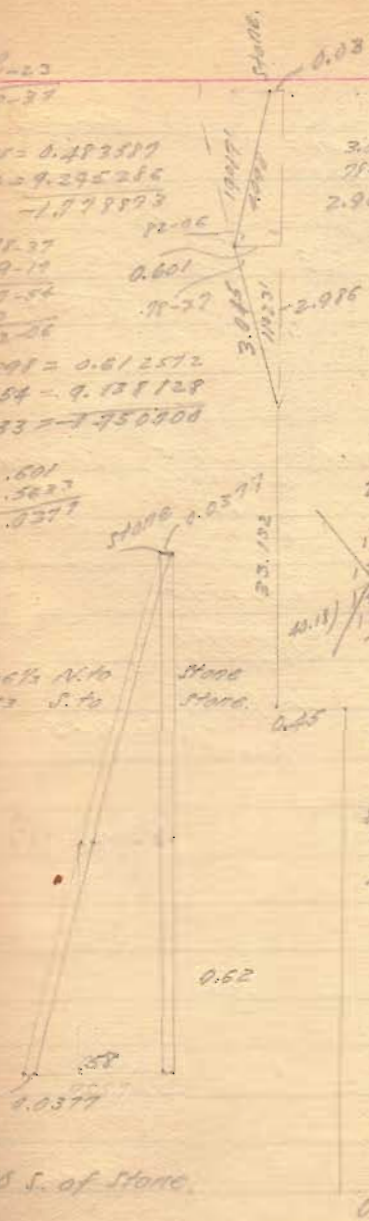
20

0.331
0.308
Correction to N.

18.425 — Stake.

10

0 — Stone. S.W. Cor. Sec. 4




3.045 = 0.483587
78-37 = 9.991372
2.986 = 0.474959

.379
.038
.341

4.098 = 0.612572
82-06 = 9.995859
4.059 = 0.608431

24.555
.58
19.440
12.775
14.248
12.454
21.940
26.090
18.290

(.354
40.18)

56.12
39.92
16.90
1.265
15.635
40.18
24.555

39.92
33.132
4.059
2.986
80.097
39.92
40.177

.50
.4938
.0062 N.

80.10
39.92
40.18

37.89
4
33.9

24.555
.62
49.110
147.330
15.224
12.054
31.701
28.026
35.550
36.144
40.18)

Stone

8.889801 : 9.040342
1.577147 = 37.77
10.617489
8.889801
53.418 = 1.727688
23
8)165

7.09
45
3545
2836
319.05

34-36½
1-51
2)36-27½
18-13-45 =

9.517335
319
9.517654

53.418
32.28
85.698 = 85.70
21.138 = 21.14

73
30
34

1.932981 : 1.325105
9.517654
10.842759
1.932981
8.909778 =

18-13-45
4-39
22-52-45
13-34-45

9.370808 : 9.773875
86
9.773961
1.508934 = 32.28
11.282895
9.370808
1.912087 = 81.67

2.15
30
85.50

0

Stone

23-25
30-13½
53-38½
19-02
34-36½

1.55
30
4.65

311754

75
9
675

211
02
4.22

180
82-58
2)97-02
T. 48-31 =

37.437
20.502
57.939
16.935

151370
154
151524

1.762904
68
1.762972

1.228657
128
1.228785
10.053446
11.282231
1.762972
48-31
18-17½ = 9.519259
66-48½
30-13½

3.61
30
10.83

9.701802
108
9.701910 : 9.996720
1.311758
11.308478
9.701910
40.42 = 1.606568

3.05
30
91.50

9.754229
92
9.754321 : 9.513375
1.151524
10.664899
9.754321
40.42
8.14
32.28 = 0.910578

9.754321

9.905925
47
9.905972
1.151524
11.057496
9.754321
20.1 = 1.343175
17.67
37.77
15.695
53.465
22.075

T. 3-09 =

15.695
17.67
33.365

10.084527
1.728070
8.356457 = 3.09
1.18
4-27
1-51

1.728029
41
1.728070

1.343802
99
1.343901
8.740626
10.084527

Arthur Bolte
Sept. 20. 1919

| | | |
|---|---|---|
| 81.49 | Stone 40' N. of Line. | |
| 80 | | |
| 70 | | |
| 68.605 | Land Line Post | |
| 61.26 | Stake. | |
| 60 | | |
| 50 | | |
| 40.84 | Stake. | Set 1/4 Stake at 40.745 |
| 40 | | |
| 30.84 | Stake. | |
| 30 | | |
| 20.415 | Nail on Stump. | |
| 20 | | |
| 10 | | |
| 0 | Stone S.W. Cor. Sec. 16 | |

| | | | | | |
|---|---|---|---|---|---|
| | | | | | |
| 80.40 | | | | | Stone. S.M. Cor. Sec. 22 |
| 80 | | | | | |
| 70 | | | | | |
| 60 | | | | | |
| 50 | | | | | |
| 40.22 | D.L. | 0°12' | | | W Stone |
| 40 | | | | | |
| 39.78 | | | | | Cor. O.S. Mg. |
| 30 | | | | | |
| 20 | | | | | |
| 10 | | | | | |
| 0 | | | | | S.E. Cor Sec. 22 |

| | | | | | | |
|---|---|---|---|---|---|---|
| 80.86 | | | | | | Stone |
| 80 | | | | | | |
| 70. | | | | | | |
| 60 | | | | | | |
| 50 | | | | | | |
| 48.943 | | | | | | Nail |
| 40.817 | D.R. 0°56' | | | | | Stake. |
| 40 | | | | | | |
| 32.817 | | | | | | Nail |
| 30 | | | | | | |
| 20 | | | | | | |
| 10 | | | | | | |
| 0 | | | | | | Stone S.W. Cor. Sec. 22 |

$T = 0°35' = 8.007809$

$1.602494 : 1.376394$
$8.007809$
$9.384203$
$1.602494$
$7.781709 = 0°21'$

35
21
14
56

$8.126 = 0.909877$
$0°56' = 8.211895$
$(-1.)\ 9.121772$
$.1324$

31.917
8.126
40.043
23.991

80.86
48.943
31.917

| | | |
|---|---|---|
| 90.795 | | Stone. |
| 80 | | |
| 72.655 | | Land Line. |
| 70 | | |
| 60 | | |
| 50 | | |
| 45.355 | D.L. 0°04' | Stone. |
| 40 | | |
| 30 | | |
| 20 | | |
| 10 | | |
| 0 | D.L. 0°41' | S.E Cor. Sec. 34 |

| | | | |
|---|---|---|---|
| 80.415 | | | Stone |
| 80 | | | |
| 70 | | | |
| 60 | | | |
| 50 | | | |
| 40.27 | O.B. 0°02' | | ¼ Stone |
| 40 | | | |
| 30 | | | |
| 20 | | | |
| 10 | | | |
| 0 | N. 30½ E. | | S.W. Cor. Sec. 33 |

80

70

60

50

41.39 — 1/4 Stone.

40

30

20

10

0 — S.W. Cor. Sec. 34

No monument found.

424
3
127.2

2.009451
127
2.009578 : 1.299943
10.351757
11.651706
2.009578
9.642122

66-01
23-41
89-42
42-20

4.21
32
125.2

45.355
41.05
86.405
4.305

2|90-09
45-04½

10.001011
125
10.001137

1.936514
25
1.936539 : 0.633973
10.001137
10.635110
1.936539
8.698571 = 45-04½
28-51½
47-56
42-13

9.827328 : 9.999999
1.613313
11.613312
9.827328
1.785984 = 61.09
41.14
102.23
19.95

180-
47-58
2|132-02
66-01

9.828301 : 9.170846
1.614264 = 41.14
11.485110
9.828301
1.656809 = 45.37

90-11
51-03
39-08

4.21
30
12.630

2) 90-15
T. 45-07½ =

10.001769
126
10.001895

45-07½
5-55½
51-03
39-12

23.38
19.00
42.38
24.38

1.627161 : 0.641474
10.001895
10.643369
1.627161
9.016208 = T. 5-55½

180
39-08
2) 140-52
T. 70-26 =
10.449248

9.800737 : 9.999996
1.278754 = 19.0
11.278750
9.800737
1.478013 = 30.06
23.35
53.41
6.71

19.41
40.43
5823
7764
7764
78.47463

1.727623 : 0.826723
10.449248
11.275971
1.727623
9.548348 = T. 70-26
19-28
89-54
50-58

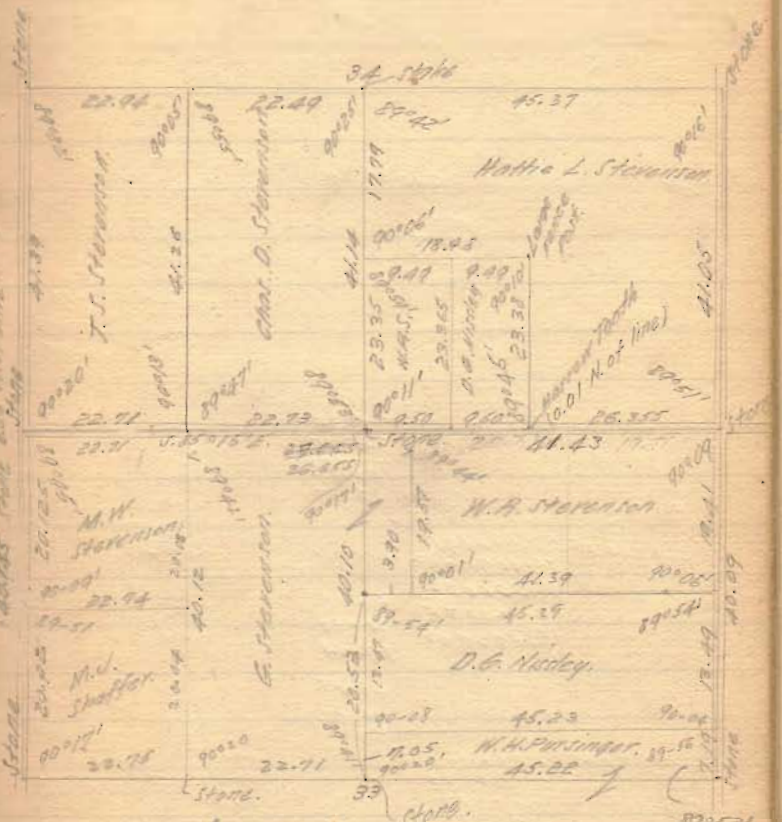
86
28
58

9.890298 : 9.800117
1.362287 = 23.35
11.168404
9.890298
1.278106 = 18.98 9.49

45.355
41.43
3.93

22.71
26.665
41.43
90.99

33-34 3-13



90.795
45.355
45.440

90-17
41-34
48-43

90-17
48-41
41-36

90-17
2)90-08
45-04

45.22
40.09
85.31
5.13

1.931000 : 0.710117
10.001011
10.711128
1.931000
9.780128 = 45-04
3-27
48-31
41-37

9.822262 : 9.999999
1.603036
1.603035
9.822262
1.770773 = 60.36
45.36
105.72
13.00

180
41-38
2)138-22
69-11

89-39
90-11
89-52
269-43
360
90-17

2.024075 : 1.176091
10.419991
11.596082
2.024075
9.572007

69-11
20-28
89-39

180-39
89-45
270-19
89-41

48-43
41-37
90-20

4.21
30
126.3

9.999992 : 9.822404
1.780773
11.603177
9.999992
1.603185 = 40.10

40.14
45.44
85.58
5.30

2)90-15
45-07½

10.001369
126
10.001895

1.932372 : 0.724276
10.001895
10.726171
1.932372
8.793799

45-07½
3-33½
48-41
41-34

9.875682 : 9.999996
1.657439
11.657434
9.875682
= 1.781752

60.50

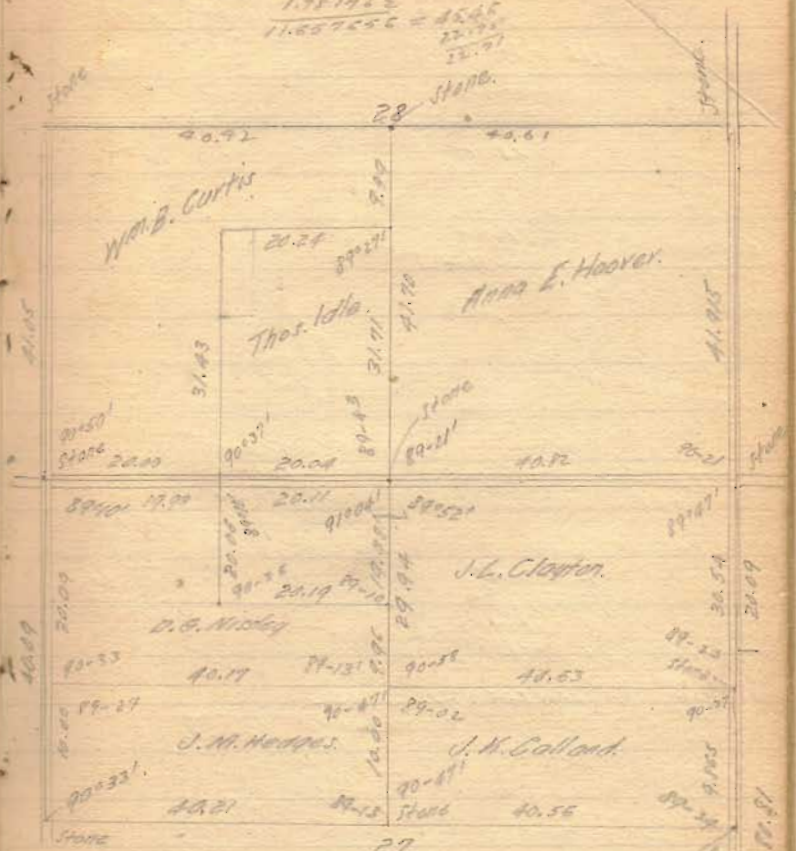
9.822120 : 9.875904
1.603185
11.479089
9.822120

1.656969 = 45.39

27-28 3-13

88-56
56
89-52

9.999993 : 9.875904
1.781752
11.657656 = 45.46
22.75
22.71

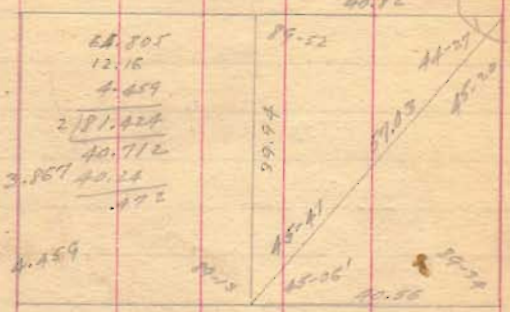



90-33
89-10
91-09
270-47

9.816361 : 9.925911
0.974051 = 9.42
10.900952
9.816361
1216 = 1.084602

9.816361 : 9.459688
0.974051
10.233739
9.816361
10.045
4.143
5.902 = .617388

89-47
44-27
45-20
180
2)124-40
67-20




64.805
12.16
4.459
2)81.424
40.712
40.24
.472

0.770999
9.816361
0.587360 = 3.867

0.770999
9.878219
0.649218 = 4.459

40.82
39.94
80.76
0.88

2)90-08
45-04

1.907196 : 1.944483
10.001011
9.945494
1.907196
8.038298

45-04
37
45-41
44-27

9.845276 : 9.999999
1.601408
11.601407
9.845276
1.756131

57.03
40.40
97.43
16.63

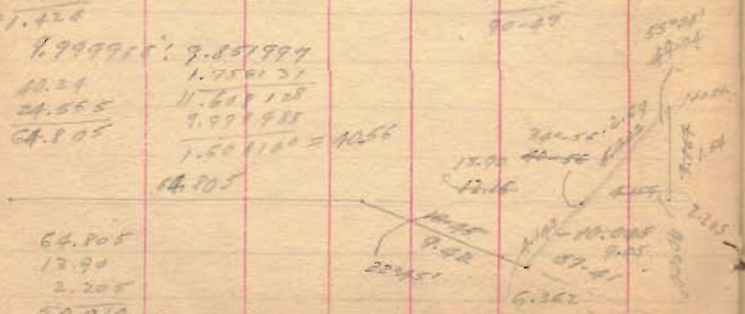
1.988693 : 1.220892
10.379213 = 7.67-20
11.600105
1.988693
9.611412

22-14
89-34
45-06
45-41
90-47

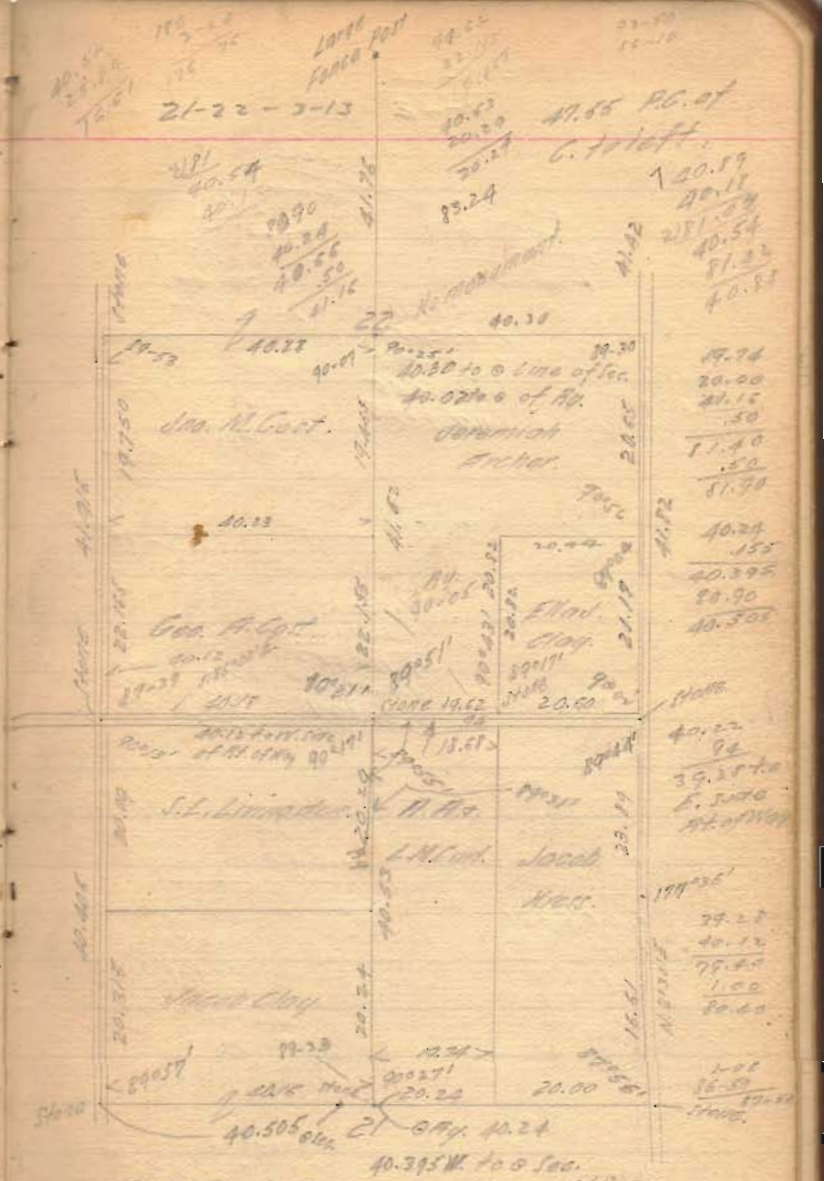
64.805
12.16
4.459
81.424

9.999988 : 9.851997
1.756131
11.608128
9.999988
1.608140 = 40.56

64.805




64.805
13.90
2.205
80.910



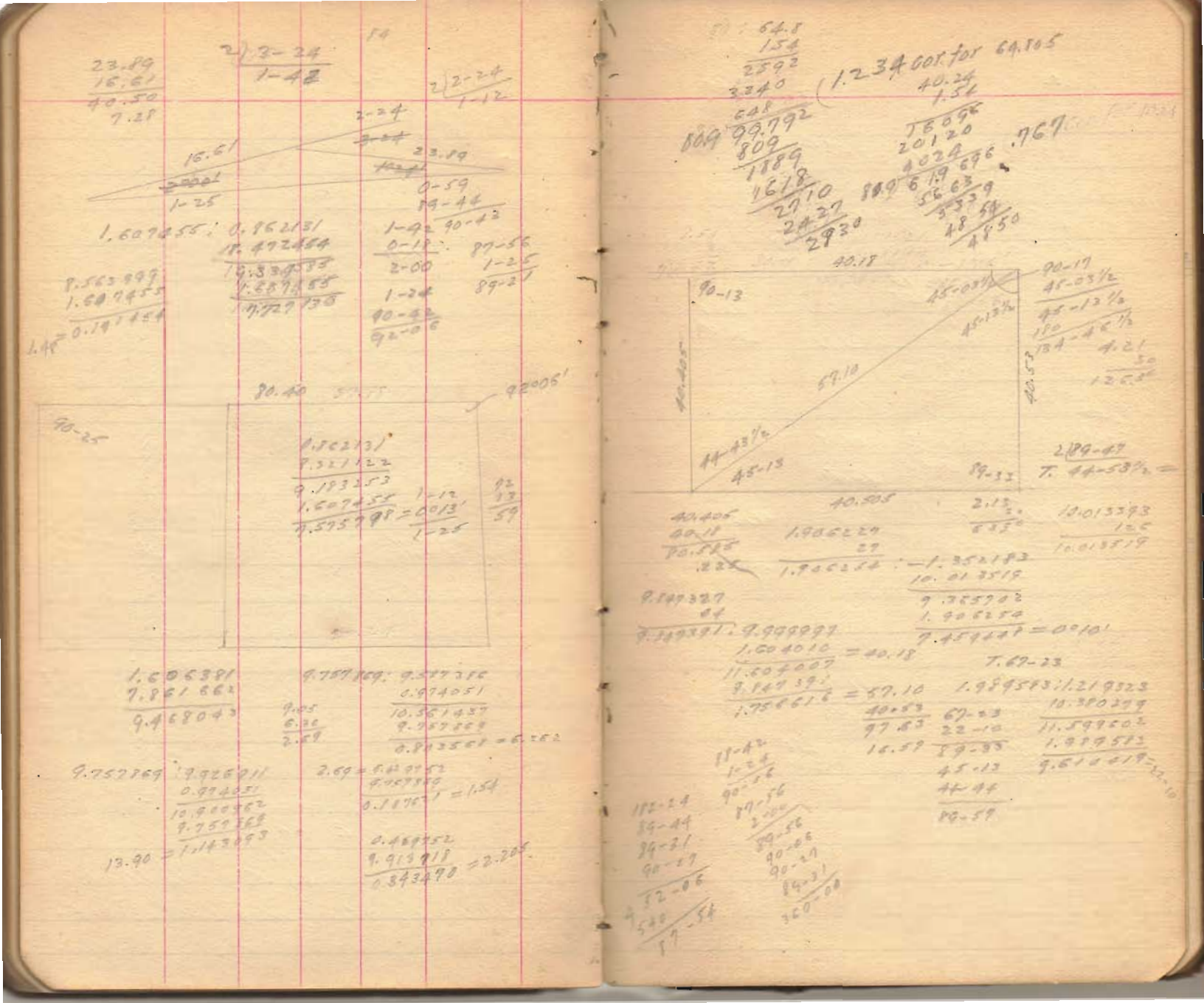

⊙ D.T. + 1. Ry. 0.44 E. of 1/4 Stone.

Width of Rt. of Way 0.50 E + W. of ⊙

81.78½ on S. Line of Sec. 21

2)81.78
40.89 1/4 Cor.

S. side (1/4 Stone) Sec. 21 N. to Cen. Sec. Ry. Spike 40.415



20.36
20.04
20.13
60.63
6.80
67.33
.27
47131
13466
81.19) 18.1791 (.224 cor. for 67.33
16228
19511
16228
32831

81.14

.66 ) 3.00 4.54
.264
360
332

.203 = -1.307496
41.50 1.618048
7.689 + 48 = 0.0171

33.80
.055
16900
16900
40.15) 1.85900 (.046
16060
25300

.35
.0454
.3046

25
.055
125
125
) 1.375 (.034
12045
1725

25.
1.29
23.71

61.15
20.44
40.71

81.13
40.84
40.29

90-10
90-36
89-28
270-24

.055
20
40.15) 1.1000 (.027
8030
29700
28105

40.71
40.17
54
108
7) 324
46
89-24
90-10

81.49
61.15
20.34

89-47
90-48
89-41
270-17
90

12

16
3
48

18
7
3) 126
42
21

3) 98
32

90-10
177-36
90-34
89-41
448-02
560
91-58

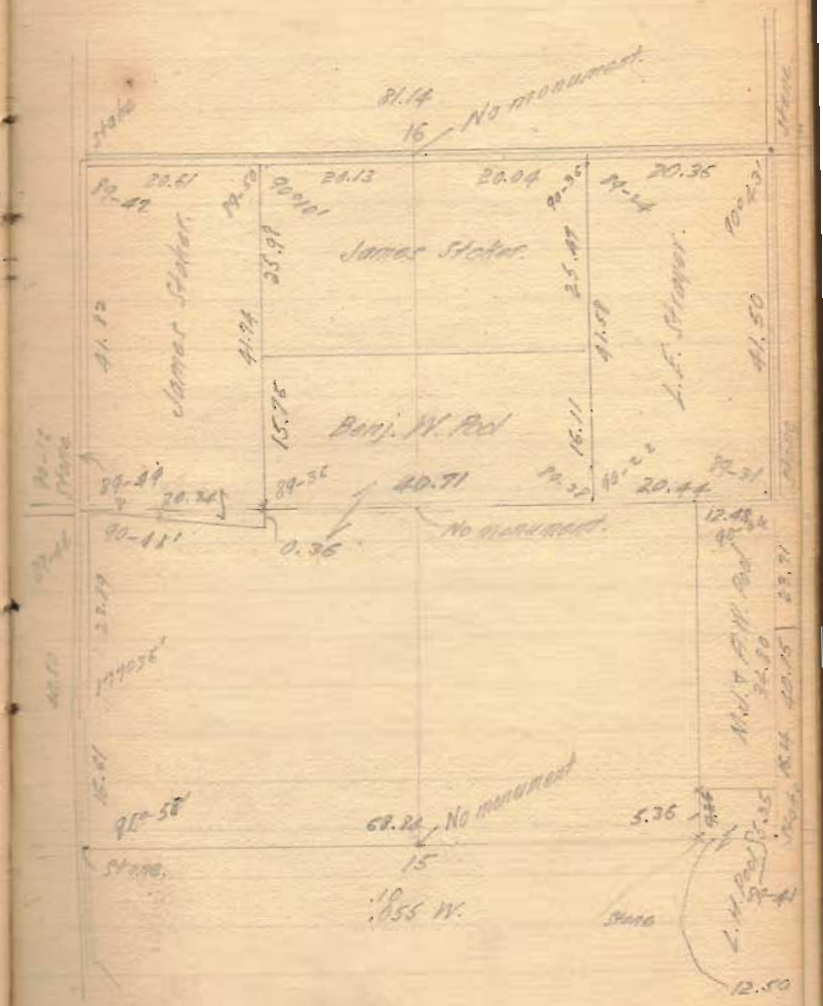
81.34
12.50
68.84

14
.103
.037 S. of Stone.

7.86
2.50
5.36

27
2
54
162
21

90-10
21
89-49



41.50
39.96
1.54
2
301
3
7)924
132

90-23
2-12
88-11
89-31
177-42
2-18

20
3
7)60
8

90-23
8
90-15

8
3
7)24
3

41.50
40.96
59
2
108
3
7)324
46

90-23
46

83
46
37

89-37
89-37
90-17
269-31
90-29

6
3
9)18
2

89-43
19
90-02

40.27
39.92
.35
2
70
3
7)210
30

89-58
30
89-28

89-42
38
90-20

2.5
2
3.0
3
9

90-18
89-23
89-59
90-20
.54

40.60
40.15
.45
90
3
7)270
38

90-01
38
89-23

89-56
90-29
89-23
269-48
90-12

16.57
16.44
.13 = -1.113943
27.54 = 1.4399.64
-3.673979 = 0.16'
7

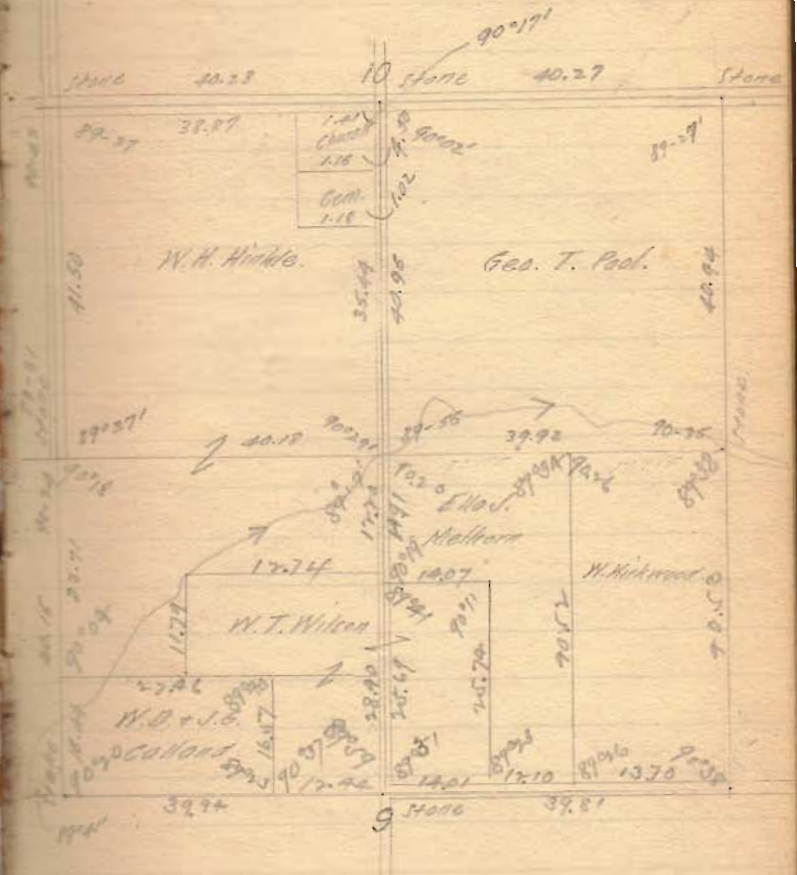
89-40

27.46
15.85
11.61

22.85
.84
9140
8004
11360
8004
3356

40.02
.023

(22



27.54
27.46
.08 = -2.903090
16.44 = 1.216902
7.687188 = 0°17'

89-40
89-23
89-56
90-20
269-39

90-37

90-49
89-07
269-39
89-59
90-37
630-11
720
89-49

.06 = -2.778151
25.74 = 1.410609
7.367542 = 0°19

16.57 = 1.219323
0°35' = 8.020021
-1.239344

.17
12.44
12.61
15.85

90-29
90-37

28.46
.13
.13

89-39
90-37
89-59
270-15

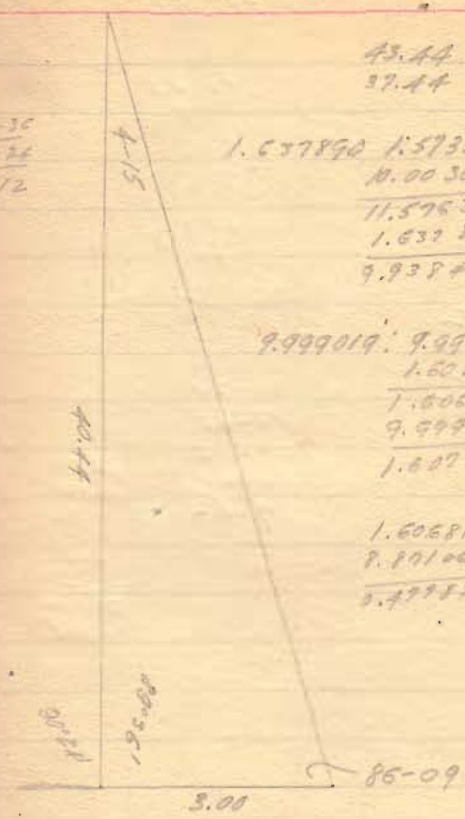
89-45
89-07

.13 = -1.113943
11.75 = 1.070407
7.043876 = 0°38'

90-23
90-11
89-31
90-37
270-19
90-53
89-41

.03 = -2.477121
28.33 = 1.452243
7.024878

.05 = -2.698970
14.07 = 1.148294
7.550676 = 0°12'




180
89-36
2)90-24
45-12

43.44
37.44

72

1.637890 1.573336
10.003032 = T. 45-12
11.576368 40-57
1.637890 4-15
9.938478 86-09

9.999019 : 9.999989
1.606811 = 40.44
1.606800
9.999019
1.607781 = 40.53

1.606811
8.871064
0.477875

40.96
3.69
37.67

40.96
40.27
81.23
.69

2/89.58
44-59
29
45-28

90.25
90.24
89-51
270-20
89-20

1.909716 : −1.838849
9.999748
9.838697
1.909716
7.928981 = 0°29'

9.852994 : 10.
1.612360
11.612360
9.852994
1.759366 = 57.46

9.852745 : 9.841640
1.612148 = 409.4
11.453788
9.852745
1.601043 = 39.91

2/89-40
44-50

40.60
39.92
80.52
.68

1.905904 : −1.832509
9.999473
9.829982
1.905904
7.924078

44-50
0-29
45-19
44-21

89-31
44-21
45-10

9.851872 : 9.999993
1.608526 = 40.60
11.608519
9.851872
1.756647 = 57.10
39.81
96.91
17.29

180
45-10
134-50
67-25
23-13
90-38
44-12

1.986369 : 1.237795
10.380992
11.618787
1.986369
9.632418 = 23-13

6
7
3/42
14

3/315
2/105
625

90-24
89-36
16
89-52

90-24
89-36

90-24
89-39
45

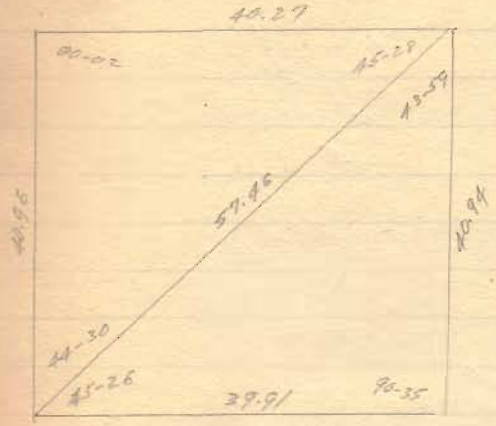
84

.38
3
7/114
16

40.44
40.245
.195

90-09

89-27
45-28
43-59
180
136-01
68-00½




57.46
40.94
98.40
16.52

606
20
191.80

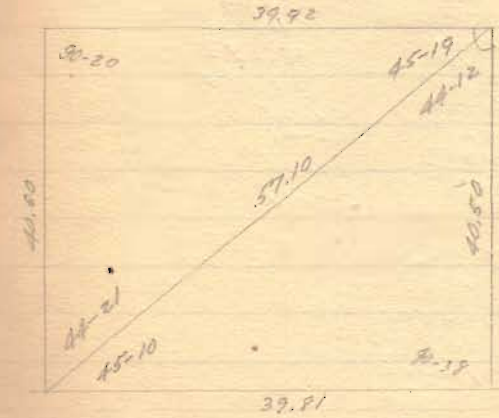
10.393590
182
10.393772

1.992995 : 1.218010
10.393772
11.611782
1.992995
9.618787

68-00½
22-34½
90-35

45-26
44-30
89-56

89-31




20
3
7/60
9

90-29
9
90-20

9.999973 9.850745
1.756647
11.607392
9.999973
[illegible] = 40.50

4.2
30
12630

40.94
40.25
81.19
.69

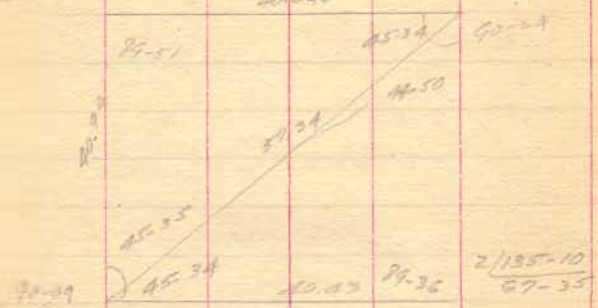
45-04½
29½
45-34

2)90-09
45-04½

10.001011
120
10.001131

1.909396 : -1.838849
10.001131
9.839980
1.909396
7.934584

40.2




2)135-10
67-35

9.853738 : 9.909999
1.612148 = 409.4
1.612147
9.853738
1.758409 = 57.34
40.945
98.283
16.395

1.992487 : 1.214579
133
1.214712
10.384565
11.599277
1.992487
9.606790

67-35
22-01
89-36
45-34

9.999989 : 9.848218
1.758409
11.606627
9.999989
1.606638 = 40.43

89-29
70-40
160-09

89-29
90-30
70-40
19-51

9.361822 : 9.925384
0.477121
10.402505
9.361822
1.040683 = 10.98

2.50
1.95
4.45

9.999982 : 9.530915
1.040683
10.571598
9.999982
1.571616 = 3.729
3.73

4.45
3.73
.72

9.999982 : 9.974792
1.040683
11.015475
9.999982
1.015493 = 10.36

| | | |
|---|---|---|
| Stone | 0.13 | |
| | .1337 | 5.205 |
| | .1459 | 21.38 |
| | .1576 | 37.19 |
| | .1600 | 40.38 |
| | .1782 | 64.93 |
| | .1857 | 74.93 |
| Stone | 0.19 | 80.70 |

40.38
35.175
5.205
.06
80.7 ) .30230 .1037
2421 13
6020
5649

40.38
.19
21.38

40.38
3.19
37.19

40.38
24.55
64.93

40.38
34.55
74.93
5.77
80.70

21.38
.06
80.7) 1.2828 .1159
807 13
4758
4035
7231

37.19
.06
80.7) 2.2314 .0276
1614
6174
5649
5250

40.38
.06
8.07 ) 2.4228 (3
2421

64.93
.06
8.07) 3.8958 .0482
3228
6678
6456
2220

74.93
.06
80.7) 4.4958 .0557
4035
4608
4035
5730

5.77
.06
8.07 ) .3462 .0416
3228 .1858
1340
807
5330

19
.06
.1858

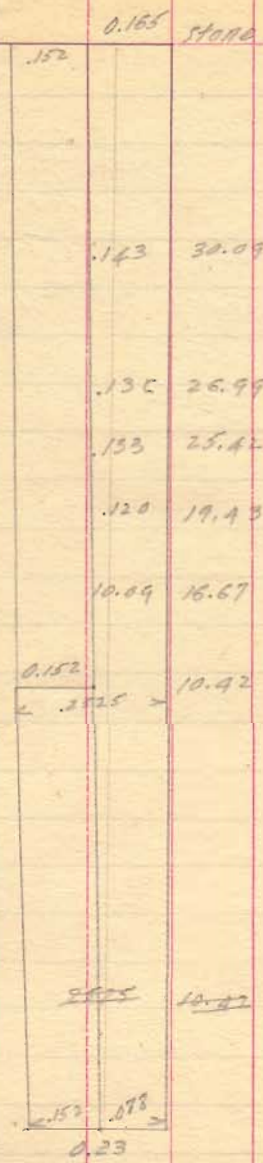
90-24
12
90-41

89-19
90-41
30
91-11
30
90-41

70
2
7) 210
20

19
.03
40.34) .5700 .014
4034
16660

.14
.66
84
84
.924
12
1848
924
11.088




0.165
0.152
0.317
0.23
.087

0.23
.152
.078

0.165
.078
.087

10.42
.087
7294

8336
40.16) .90654 (.0225
8032
10334
8032
23020

.0225
.078
.152
.2525

19.43
.087
13501
15544
40.16) 1.68941 (.042
16064 .078
8301 .120

16.67
.087
11669
11338
40.16) 1.25049 (.031
12048 .078
4569 .109

25.42
.087
17794
20336
40.16) 2.21154 (.055
20080 .078
20354 .133

27
.087
189
216
40.16) 2.3496 (.058
20080 .078
34100 .136

30.09
.087
21063
24072
40.16) 2.61783 (.065
24096 .078
20823 .143

.165
.152
.317
.23
.087
2
.174
3
7) .522
7
89-38
89-45