

12

E. D. Garwood	axe	2
J. W. Embrey	Sledge	2
Pearl Garwood	Sledge	1 $\frac{1}{2}$ $\frac{1}{2}$ $\frac{1}{2}$
Marion Shellabarger	H. ch.	2
Peter Hudson	Wagon	2
Blaine Heath		2
A. R. Richey	R. ch.	2
James Reams		$\frac{1}{2}$
Elmer Johnson	$\frac{1}{8}$ $\frac{1}{2}$	$\frac{1}{2}$ $\frac{1}{2}$
F. J. Reams	S. stakes	$\frac{1}{2}$
✓ Dan Lippincotte	Rig	
Don Wonders	III	1
Driscoll Wonders	II	

## Road 10 Jefferson - Perry

## Bristle Ridge Pike

B.M.		29.95			
X	5.47	35.44			
0	5.70	29.74			
S. Side	6.50	25.90			
1	4.00	31.44			
S. Side	4.60	30.84			
2	6.50	28.98			
N. Side	7.00	28.44			
S. n	6.40	29.54			
3	8.60	26.84	$\frac{10.40}{18}$	N. side	
4 T.P.	10.48	24.96	$\frac{11.80}{20}$	N. side	
X	0.98	25.94	$\frac{10.50}{23}$	S. side	
B.M.	3.50	22.44			
4.58					
N. Side W	4.30	21.64			
5	3.85	22.09	$\frac{3.80}{5}$	$\frac{6.00}{18}$	to Right
			$\frac{3.80}{8}$	$\frac{4.70}{14}$	to Left
			$\frac{4.80}{6}$	$\frac{7.20}{13}$	
6	4.80	21.14	$\frac{4.80}{9}$	$\frac{6.70}{16}$	$\frac{5.10}{25}$
			$\frac{5.00}{10}$	$\frac{6.70}{16}$	
7	5.00	20.94	$\frac{6}{6}$	$\frac{12}{12}$	
			$\frac{5.00}{10}$	$\frac{7.70}{16}$	$\frac{6.00}{25}$
8 T.P.	6.01	19.73	$\frac{6.00}{7}$	$\frac{7.70}{12}$	
X	7.79	27.72	$\frac{6.00}{8}$	$\frac{8.30}{15}$	$\frac{7.30}{21}$
S. End 48	9.70	18.02			
N. End					

B.M. <sup>Ballinger's</sup> cement walk at front porch.

Sta. 0 in 0 Ballinger pine in East Liberty.

N. 79 E. ?

S.S. 30 L.

Sta. 2 + 71 Line between Ballinger and Ballinger East line school lot 0 + 40

Line Ballinger & Shellabarger 3 + 66

Sta. 6 + 55 Line between Shellabarger and Fyke

B.M. 0 porch floor Shellabarger

7 + 36 W. Line School lot

Sta. 8 Angle N 77° 15' W. stakes in old road

Sta. 9 + 74 Line between Bell and cemetery

X		<u>27.17</u>		
9	7.10	20.62	7.10 7	8.40 11 12.50 16
10	4.50	23.22	7.10 8 4.50 14 4.50 9	10.20 21 7.50 26 0.30 26 6.00 19
T.P.	0.26	27.46		
X	13.00	<u>40.46</u>		
11	8.90	31.56	10.20 16 10.60 15	5.60 26 8.50 22
12	1.55	38.91		
13	0.70	38.21		
14	0.60	39.86		
15 T.P.	1.08	39.38		
X	12.58	<u>51.96</u>		
B.M.	9.96	42.00		
16	13.20	35.76		
17	12.40	39.36		
18	10.80	41.16		
17	6.40	45.56	8.00 14 7.50 18	4.70 21
19+85	3.00	48.96		

Sta. 10 - Angle N. 73° 30' W.

Sta. 11 - Angle N. 59° 00' W.

12 + 50 Cemetery Gate

Sta. 16 + 60 Line between Bell and Cemetery on N.

B.M. Top Josiah's headstone apr-15

17+85 Bell's driveway

1		<u>51.96</u>		
20	3.60	48.36	1.20 25 <u>3.60</u> 15	0.00 28 2.70 21 <u>8.00</u> 24
21	8.00	43.96	15	
22	7.20	42.76		
23	7.60	44.36		
24	5.20	46.76		
T.P.	1.10	50.86		
25	12.15	<u>63.01</u>	6.50	3.40
	8.50	55.51	12	21
T.P.	0.57	<u>62.44</u>	15	5.50
				24
26	9.64	<u>72.08</u>	8.40	4.60
	8.40	64.68	11	17
			8.40	5.50
			12	17
B.M.	4.56	69.52	4.80	3.50
27	4.77	67.31	12	18
28	3.30	68.98		
29 T.P.	1.78	70.30		
30	12.70	<u>83.00</u>		

Sta 20 - Angle N. 87° 00' W.

20+70 - 12' to bank on N.

22+50 Flat-top Span

Sta. 27 - Angle N. 77° 15' W.

B.M. 12" Walnut N. 27

Sta. 29+59 Line between Bell and Armstrong on N. Birmingham and Armstrong on S.

T		<u>83.10</u>			
30	8.20	74.80			
J/	1.10	81.90	$\frac{1.10}{9}$	$\frac{3.60}{11 \text{ to } 20}$	$\frac{0.40}{24}$
T.P.	0.77	82.21	$\frac{1.10}{16}$	$\frac{2.70}{22}$	$\frac{\text{high}}{30}$
T	12.72	<u>94.93</u>			
32	6.90	88.03	Level		
B.M.	3.75	90.98	$\frac{6.90}{9}$	$\frac{8.60}{14}$	$\frac{5.00}{22}$
33	1.30	93.63	Level		
T.P.	0.45	94.48	$\frac{1.30}{10}$	$\frac{3.00}{13}$	$\frac{-0.60}{19}$
T	11.16	<u>105.64</u>			
34	7.30	98.34	$\frac{7.30}{10}$	$\frac{9.10}{15}$	$\frac{9.10}{15}$
			Level		
35	2.70	102.94	$\frac{2.70}{22}$	$\frac{1.00}{25}$	
			$\frac{1.70}{14}$	$\frac{2.00}{20}$	
T.P.	0.69	104.95			
T	11.50	<u>116.45</u>			
36	8.40	108.05	Same as 35		
			" " "		
37	3.60	112.85	$\frac{3.60}{11}$	$\frac{1.70}{22}$	
T.P.	1.05	115.40	$\frac{3.60}{13}$	$\frac{1.70}{20}$	
T	11.77	<u>127.17</u>			
38	9.80	117.37		$\frac{2.00}{22}$	
B.M.	5.06	122.11	Level		
39	4.80	122.37			

B.M. 10" Walnut N. 32

B.M. 10" Sugar N. 38.

$\pi$		<u>127.17</u>		
T.P.	0.47	126.68		
$\pi$	12.88	<u>139.56</u>		
40	12.20	127.36	$\frac{12.20}{13}$ $\frac{12.20}{15}$	$\frac{7.90}{27}$ $\frac{11.20}{27}$ N. side S. side
41	7.80	131.76	Same as 40	
42 T.P.	2.70	136.86	"	"
$\pi$	12.67	<u>149.53</u>	"	"
43	6.90	142.63	Level	
			$\frac{6.90}{14}$	$\frac{5.40}{23}$
44	2.80	146.73	Same as 43	
T.P.	0.47	149.06	"	"
$\pi$	6.65	<u>153.71</u>		
45	5.60	150.11	"	"
450	3.75	151.96		
B.M.	3.70	152.01		
46	4.10	151.61	"	"
47	5.10	150.61	"	"

Sta. 45 - Angle. N. 76° 30' W.

24" Oak near sta. 46

155.71

T				
48	7.80	147.91	Level	
			"	
T.P.	9.85	145.86	"	
T	9.20	133.06		
49	10.90	144.16	Level	
			"	
50	11.70	143.36	"	
B.M.	11.10	144.96		
51	9.50	146.56	"	
			5.26	3.95
52.T.P.	5.26	149.80	18	24
			5.26	4.03
T	5.42	155.22	13	22
T.P.	1.50	153.72		
T	12.01	165.73		
			9.80	8.20
53	9.80	153.93	15	24
			2.50	2.40
			14	24
			4.60	
54	4.60	161.13	30	
			24.00	
54+55 1/2	2.04	163.69	30	
			4.30	.26
55	4.30	161.48	9	27
			4.30	2.80
			12	35
			12.5	4.20
56.T.P.	10.48	155.31	7	25
			10.5	11.60
T	8.62	163.93	9	25
			10	30
57	10.40	153.53	8	30
			10	
B.M.	10.32	153.61		
			8.80	above road
58	9.90	154.53	8.40	27
			8	30

Sta 50+40 - wooden box 15x24

o Driveway 7.40 S, 53

Sta. 54+55 1/2 - Angle N. 95° 15' W.  
(Armstrong's house)

B.M. 30" white oak N. 50+50  
54+36 Center gate Armstrongs 100

57+90' Bridge 18' span 240  
B.M. on N.W. cor N.W. abutt. of bridge  
on cement coping.

T		<u>163.93</u>		
59	7.00	156.93	$\frac{7.00}{7}$	$\frac{7.00}{26}$
			$\frac{7.00}{10}$	$\frac{5.70}{25}$
60 T.P.	3.20	160.73	same	
T	13.00	<u>173.73</u>	"	
61	9.90	163.83	Level	
62	6.00	167.73	"	
63 T.P.	1.80	172.93	"	
T	10.56	<u>183.79</u>	$\frac{0.83}{11}$	$\frac{5.10}{19}$
63+35	4.30	179.49		
64	4.10	179.69	Level	
T.P.	1.85	181.94		
T	8.82	<u>190.76</u>		
65	6.60	184.16	Level	
			$\frac{6.60}{10}$	$\frac{3.80}{16}$
66 T.P.	1.74	189.02	Level	
T	11.85	<u>200.87</u>	$\frac{1.90}{13}$	$\frac{.50}{14}$
B.M.	5.63	195.24		
67	7.30	193.57	same 66	
68	4.20	196.67	"	
69 T.P.	1.40	199.97	"	
T	12.31	<u>211.78</u>	"	

Sta. 61 + 90 Line between  
Armstrong and Williams on S.

→ Gate Elmer Williams

Sta. 64 + Stone on line  
Armstrong and Johnson on N.

Sta. 66 + 69. W. corner school lot  
→ B.M. 30" Walnut S. 2250'



π		<u>211.78</u>	
70	9.90	201.88	Same 66
71	7.90	204.38	" "
72	5.10	206.88	" "
73 T.P.	1.30	210.48	Level
π	12.10	<u>222.58</u>	
74	7.40	215.18	" "
75	5.40	217.18	5.40 6.5 8 1.5 7.02 7.0 <u>16</u> Level
76 T.P.	2.00	220.58	Level
π	10.91	<u>231.49</u>	
77	5.10	226.49	5.00 2.4 7.3 2.0 5.00 3.70 1.6 2.2
78 T.P.	1.01	230.48	Level
π	11.45	<u>241.93</u>	
79	8.40	233.53	9.50 6 Level
B.M.	7.01	237.92	

Sta. 77 - Angle N. 75° 15' W.

B.M. 30 oak S. 79+90

7.

T 241.93

80 5.00 236.93

81 6.00 235.93

81+50 6.60 235.33

82 7.90 234.53 Level

82+36 7.10 234.83

83 5.60 236.33 "

84 3.60 238.33 "

85 T.P. 0.86 241.07

T 12.50 253.57

86 8.70 244.87

86+69 5.70

87 4.30

87+27 1.10

T.P. 2.50 251.07

T 10.36 261.93

88 4.70 2.40 2.00

1.9

4.70 1.30 22

7.2 30

88+50 T.P. 7.60 253.83

T 10.70 264.53

→ @ Dinscroy Argo's  
Sta 81+44 Line between  
Johnson and Stewart, on N.  
Box Culvert 12"

Sta 85+61 Line between  
Argo and Johnson, on S.

→ @ Stewart's Driveway

→ @ R.F. Johnson Driveway

→ Bank on each side

89	5.70	5.70	2.10
		<u>1.4</u>	25
		5.70	2.10
		<u>1.2</u>	22

90 5.10 Level

91 3.00 "

T.P. 2.05 262.48

π 11.50 273.98

B.M. 8.50 265.48

92 8.50 "

T.P. 1.25 272.73

π 7.90 280.63

93	6.40	6.40	2.20
		<u>9</u>	27
		6.40	4.30
		<u>24</u>	30

94 5.10 Level

94+50 5.10

95 3.90

96 T.P. 1.52 279.11

π 12.20 291.31

97	7.80	7.80	5.00
		<u>13</u>	21

Level

98 T.P. 1.55 289.76

π 5.20 294.96

99 4.50 Level

Sta. 90-Angle. N. 74° 15' W.  
 Sta 90+95 hinge between  
 Stewart and Reams  
 Sta 91+63 hinge between  
 Johnson and Reams

Box white oak N. 91+75'

Box culvert 9' x 18'

100	5.00	5.00	5.40
		12	27
		Level	
101.	5.00		"
101 + 50	5.00		"
102	3.10		"
100 T.P.	3.62	291.34	
π	2.92	<u>294.26</u>	
104	5.10		"
105 T.P.	8.56	285.70	8.56 5.70
			13 27
π	.55	<u>286.25</u>	Same
B.M.	2.65		
106	8.04		Level
107 T.P.	10.72	276.53	
π	3.60	<u>279.13</u>	
108	7.70		"
108+15	7.70		
109	8.20		

Box culvert 5x12

Sta 105 Line between Jefferson and Perry townships.

→ B.M. White oak N. 105 + 50

→ 124 stone culvert  
 Sta. 108 + 15  
 between Reams and  
 townships on S.  
 Joslyn and Reams on N.

110 T.P. 2.81 276.32 Level

$\Sigma$  9.34 285.66

T. P. 0.85 274.81

$\Sigma$  12.51 297.32

111 11.20

$\frac{11.20}{12} \quad \frac{6.40}{23}$   
 $\frac{11.20}{11} \quad \frac{4.60}{24}$

112 3.10

$\frac{3.10}{10} \quad \frac{6.20}{20}$   
 $\frac{3.10}{14} \quad \frac{2.30}{10}$

113 2.60 Level

114 3.50 "

115 T.P. 3.75 293.57

$\Sigma$  7.10 306.67

115+10 7.10

116 6.00 "

116+62 2.61

$\frac{7.60}{14} \quad \frac{3.90}{19}$   
 $\frac{7.60}{16} \quad \frac{7.20}{15}$

117 7.00

118 P.T. 12.90 287.77 Level

$\Sigma$  6.90 294.67

118+75 4.30

118+85 11.20

$\frac{11.20}{9} \quad \frac{10.20}{16}$   
 $\frac{11.20}{7} \quad \frac{10.20}{14}$

119 6.30

to 118+39 angle N. 79° 45' W

to 115 angle S. 84° W

to Box subject 14+15

to 116+62 Jamison Road.

on North side

to Jamison pike

to subject 5.18"

to Box 2.16 x 20"

120 T.P.	1.05	293.62	1.05 8	3.60 19	
T	10.45	304.07	1.05 9	2.10 23	
121 T.P.	1.30	302.77	1.30 11	0.50 16	-5.00
T	12.00	314.77	1.30 14	0.20 17	25 5.00
B.M.	4.25	310.52			
122	6.30		6.30 14	4.70 17	
			6.30 14	5.30 14	
123	2.50		Level		
			"		
124	2.30		"		
			"		
125	2.30		"		
			"		
126 T.P.	5.15	309.62	"		
T	8.70	318.32	"		
126+60	9.70		"		
127	8.50		"		
			"		
128	6.30		"		
			"		
129	4.80				

Black walnut N. 121+30 N

122+25 Angle S. 85° 00' W.

30x culvert.

130	4.70		Level
131	3.30		"
132 T.P.	0.45	317.87	"
π	7.56	<u>325.43</u>	
132+60	3.10		
133	3.80		"
134	8.00		
		<u>8.00</u>	<u>9.50</u>
		6	30
		<u>6.00</u>	<u>10.30</u>
		5	13
134+40	11.2		
B.M.	8.20	317.23	
135	7.00		
		<u>7.00</u>	<u>3.50</u>
		12	25
			Level
136 T.P.	2.00	323.43	
π	11.90	<u>335.33</u>	
		<u>11.9</u>	<u>10.60</u>
		15	21
			Level
137	8.70		
		<u>8.70</u>	<u>4.00</u>
		15	24
			Level
138	4.80		
		<u>4.80</u>	<u>2.90</u>
		13	18
139 T.P.	8.6	334.47	Level
π	12.40	<u>346.87</u>	"

→ 5 beams yard No.  
 132 Angle - S. 84° 15' W

10" pipe culvert S. end  
 B.M. 36" W. oak S. opp 135

→ 139+91 Prop. line between  
 J. F. Ream and Mrs. Ball  
 on North

140	6.65	<u>6.65</u>	<u>5.30</u>
		14	21
140+30	9.70	Level	
141	2.30	"	
142 T.P.	2.00	344.87	
T	8.80	<u>353.67</u>	
143	8.20	"	
144	5.50	"	
145	7.20	"	
146	7.60	<u>7.60</u>	<u>7.60</u>
		7	30
		<u>7.60</u>	<u>8.50</u>
		7	13
147	6.90	Level	
148 T.P.	4.20	349.43	
T	12.90	<u>362.33</u>	
149	6.50	<u>6.50</u>	<u>5.50</u>
		18	21
		<u>6.50</u>	<u>7.00</u>
		17	27

3 Crosssaddle's Driveway

149+55.6" - Angle S. 83° 15' W



149+60	3.30	Level	
		$\frac{3.30}{16}$	$\frac{0.6}{22}$ - $\frac{2.50}{30}$
150	3.10	Same	149+60
151 T.P.	5.92	356.41	Level
$\pi$	0.74	<u>357.15</u>	"
B.M.	2.00	355.15	
152	4.60		$\frac{3.20}{18}$ Level
153	7.2		
	10.10		
153+75	7.30		
154	6.70		$\frac{6.90}{30}$ $\frac{6.70}{18}$ $\frac{8.4}{20}$
opp. 154	7.70		
155 T.P.	4.90	352.25	Level
$\pi$	10.15	<u>362.40</u>	Same 154
156	5.70		Level
			"
157	2.70		"
158 T.P.	0.55	361.85	"
$\pi$	5.01	<u>366.86</u>	"
159	4.50		"

Sta. 151+46 Line between  
 E.M. & W. car. poor side of Burdigs Schoolhouse  
 Clapsaddle and Schoolhouse  
 on South side

Sta. 152+66.6 Line between  
 Adams Lane opp 152  
 Clapsaddle and Adams  
 on North side  
 B. Curle's lane

12" x 12" box culvert bend  
 Sta. 157 - Angle S = 87° 15' W.

157+44	4.80		
B.M.	2.15	364.71	
160 T.P.	4.95	364.91	Level
π	1.41	<u>363.32</u>	
161	3.90		3.90 5.10
			7 9
			<u>3.90</u> 4.50
			11 14
162	6.30		same 11
			"
162+75	8.20		"
163	6.20		"
			"
164	5.40		"
			"
165	6.10		"
			"
166 T.P.	5.50	357.82	"
π	3.50	<u>361.32</u>	
167	4.70		Level
			"
168	5.70		"
			"
			"
169	4.30		"
			"

clapsaddle's yard gate

~~To 160+20~~ Angle N. 85° 15' W.  
(Clapsaddle's House)

~~24 W. cot door side of house~~  
(161-172)  
changed the step from side to  
center of road.

14x12" Box culvert

170	2.70		Level
171 T.P.	1.94	359.38	"
π	6.99	<u>366.38</u>	
172	5.90		$\frac{5.90}{10} = \frac{4.70}{12}$
T.P.	11.04	355.31	same
π	0.85	<u>356.16</u>	
173	3.40		Level
174	5.60		"
175	6.10		"
176	5.80		
177 T.P.	3.02	353.14	"
π	1.12	<u>354.26</u>	
178	6.60		"
Opp. 178	10.20		
B.M.	7.60	346.66	
179	9.50		"

Sta 172+36 Angle S. 80° 30' W

Sta. 172+75 Line between  
Clapsaddle and Farney on South  
Clapsaddle and Elliot on North

From sta. 175 S. stakes 30' to N

B.M. S.E. cor lower step of Elliotts patch  
D. Elliotts Gate Way N.  
Sta. 178+03'6" Angle S. 85° 30' W.

180 T.P.	11.10	343.16	Level
T	6.20	<u>349.36</u>	
181	6.40		$\begin{array}{r} 6.40 \\ 6 \\ \hline 9.10 \\ 14 \\ \hline 16 \end{array}$
T.P.	3.52	345.84	
T	8.90	<u>354.74</u>	
182	7.70		$\begin{array}{r} 7.70 \\ 19 \\ \hline 11.30 \\ 28 \\ \hline 28 \end{array}$
			Level
183	7.50		$\begin{array}{r} 7.50 \\ 15 \\ \hline 9.20 \\ 30 \\ \hline 25 \end{array}$
184	10.70		Sqm < 183
			"
185 T.P.	12.40	347.34	
T	3.54	<u>345.84</u>	
186	7.70		$\begin{array}{r} 7.70 \\ 16 \\ \hline 4.10 \\ 24 \\ \hline 24 \end{array}$
			Level
187 T.P.	12.45	339.39	
T	2.95	<u>336.34</u>	Level
188	7.05		$\begin{array}{r} 7.05 \\ 31 \\ \hline 9.05 \\ 12.10 \\ \hline 23 \end{array}$
188+36	10.70		
189	8.65		Level
			"

Sta 183 Angle S. 75° 15' W.

Side of slide

Sta 185+22 Angle S. 66° W.

Back of N. slide between 185 & 186

Sta 182+27 Angle S. 61° 30' W.  
Stage  
2219 Box culvert

190	5.70		5.90 16 30 180	1.80 30 5.01 22	
190+40	4.50				
B.M.	0.60	335.74			
191 T.P.	3.60	332.74	Level		
π	8.85	<u>341.59</u>	"		
192	5.50		5.50 15	0.5 27	-1.5 30
192+45	7.10		Level		
193	4.50		4.50 21 4.50 8	0.2 280 6.60 16	-1.3 30
194	3.60		Level		
			"		
195	4.60		"		
			"		
196	4.50		"		
			"		
197 T.P.	2.90	338.69	"		
π	9.12	<u>347.81</u>	"		
198	5.20		"		
			"		
199	5.70		"		
			"		

→ → O Stanley Driveway  
 → → B.M.  30" Walnut N. 190+90

O Piper Driveway

Sta 197+92 Angle S. 63° 45' W.  
 line between Brawly and  
 Gerwood on S.

200 T.P.	4.22	343.59	LEVEL
T	2.50	<u>346.39</u>	
201	4.90		"
201+25	6.30		"
202	4.70		"
203 T.P.	3.30	343.09	"
T	5.10	<u>348.19</u>	"
204	5.10		"

205	7.30	
<sup>B.M.</sup> 205+25	9.80	340.39

206 T.P.	8.85	339.34	5.55	6.60
T	2.50	<u>341.84</u>	15	26
207	6.30		8.85	8.20
			12	25
			6.50	2.60
			14	26
			6.30	3.80
			16	23
			11.00	7.20
			15	25

208 T.P.	10.95	330.39	11.00	10.60
T	1.20	<u>332.09</u>	9	15
208	6.90		6.90	1.30
T.P.	11.45	320.64	18	30
T	2.11	<u>322.75</u>	6.90	5.20
210	6.60		13	22

			6.60	0.90
			19	30
			6.60	4.00
			11	20

Sta 199+50 Angle S. 78° 30' W.  
 to Pine Johnson Gate way

Sta 201 Angle S. 84° 00' W.

→ E.M. 15" Walnut S.  
 Sta 205+62 Pine Johnson  
 and Maddox on N.  
 Sta 203+55 Pine Garwood  
 and Maddox

T.P.	11.62	311.13		
T	1.91	<u>313.04</u>	3.50	1.20
211	3.81		22	30
			<u>3.50</u>	<u>2.70</u>
			10	22
			<u>9.25</u>	<u>7.60</u>
212 T.P.	9.25	303.79	25	30
T	1.11	<u>304.90</u>	<u>9.25</u>	<u>2.90</u>
			7	30
213	6.00		Level	
			6.00	1.50
			12	27
214	8.20		<u>8.20</u>	<u>10.10</u>
			14	30
			<u>7.20</u>	—
			30	
215	8.60		Level	
			"	
216 T.P.	7.90	297.00	"	
T	6.30	<u>303.30</u>	"	
217	5.30		"	
			6.20	9.70
218	6.20		9	30
			<u>6.20</u>	<u>3.20</u>
			17	24
			6.80	12.40
219 T.P.	6.80	296.50	4	30
T	4.50	<u>301.00</u>	<u>6.80</u>	<u>4.00</u>
			20	26

Sta. 209 Angle S. 83° 00' W.

Sta. 213 + 19 Angle S. 76° 30' W.

Sta. 218 Angle S. 80° 15' W.

220 3.00  $\frac{3.00}{17} \frac{2.70}{30}$   
 $\frac{3.00}{21} \frac{1.00}{30}$

221 3.20 SAME 220

222 8.60  $\frac{8.60}{15} \frac{5.80}{30}$   
Level

T.P. 10.15 290.85  $\frac{91.7}{15.5}$

T 0.50 291.35

223 3.60  $\frac{6.30}{30}$

223/224 Level

224 4.80 Level

224 3.32 288.03

225 T.P. 11.50 299.85  $\frac{11.50}{4} \frac{10.3}{22}$

T 1.97 281.82 Level

226 T.P. 8.61 273.21  $\frac{8.61}{6} \frac{6.30}{18}$

T 1.04 274.27 Level

227 7.10 "

T.P. 11.40 262.87 "

T 1.24 264.11

228 4.90

229 T.P. 10.85 253.24 "

T 1.15 254.41

Sta 219+82 Angle N. 89° 30' W.

Sta 222+20 Angle N. 85° 00' W.

→ RM 12<sup>th</sup> Locust S.

Sta 224 Angle N. 75° 30' W.



230 T.P.	8.55	245.56	Some	
T	2.06	247.62		
231 T.P.	8.60	239.02		
T	0.80	239.82		
232	5.30			5.30 13 5.30 22
				8.70 30 1.50 30
233 T.P.	9.07	230.75	Level	
T	1.54	232.59		9.07 16 8.21 19 18.01 13
B.M.P.	8.90			5.20 30 7.60 38 3.70 30
234 T.P.	8.31	224.28		
T	2.15	226.43		
235 T.P.	10.35	216.08		10.35 17 10.08 14
T	2.16	218.24		8.10 30 6.30 30
236 T.P.	9.65	208.59	Level	
T	1.20	209.79		9.65 15 7.20 16
237 T.P.	7.20	202.59	Level	
T	2.00	204.59		7.20 30 5.40 30
238 T.P.	8.50	196.09	Level	
T	1.70	197.79	"	
238+50	5.80			5.80 20 5.80 22 10.25 28 10.25 21
				7.20 30 1.30 30 10.6 30 4.30 30
239 T.P.	10.25	187.54		
T	1.45	188.99		

Sta. 532+30 Angle N. 75° 30' W  
 Line between Geo Piper  
 and G. W. Maddox on N. side  
 B.M. 36 sugar N. 238

Sta. 234+84 Angle N. 82° 00' W.  
 234+84 line between Maddox  
 and Williams on South side

239 <sup>T.P.</sup>	6.25	180.74	<u>6.25</u>	<u>7.40</u>	
π	1.58	<u>184.62</u>	16	<u>2.60</u>	$-\frac{1.40}{30}$
240 T.P.	7.44	197.18	<u>7.44</u>	<u>9.60</u>	
π	1.35	<u>178.53</u>	20	<u>3.00</u>	
240 T.P.	12.40	166.13	<u>7.44</u>	<u>2.90</u>	
π	1.95	<u>168.08</u>	22	<u>3.00</u>	
241	3.70		3.70	<u>9.00</u>	
			20	<u>3.00</u>	
			<u>3.70</u>	<u>0.70</u>	$-\frac{2.00}{30}$
			13	<u>4.7</u>	
241+50 T.P.	8.90	159.19	Same		
π	1.94	<u>161.12</u>			
242 T.P.	9.42	151.70	<u>7.42</u>	<u>7.00</u>	
π	1.34	<u>153.04</u>	20	<u>3.00</u>	
			<u>9.42</u>	<u>6.10</u>	
			20	<u>3.00</u>	
242+50	6.50		<u>6.50</u>	<u>4.50</u>	
			19	<u>3.00</u>	
			<u>6.50</u>	<u>4.20</u>	
			24	<u>3.00</u>	
			<u>12.50</u>	<u>12.30</u>	
243 T.P.	12.55	140.99	17	<u>3.00</u>	
π	1.35	<u>141.84</u>	24	<u>5.10</u>	
			<u>12.55</u>	<u>8.60</u>	
243+50 T.P.	8.10	133.74	17	<u>3.00</u>	
π	7.40	<u>151.14</u>	17	<u>4.20</u>	
B.M.	12.75			<u>3.00</u>	
244 T.P.	9.50	131.64	<u>9.50</u>	<u>8.60</u>	
π	0.88	<u>132.52</u>	19	<u>3.00</u>	
			<u>9.50</u>	<u>7.00</u>	
			22	<u>3.00</u>	
244+50 T.P.	8.11	124.41	Level		
π	0.90	<u>125.31</u>			
245	5.30				

239+19 Angle S. 82° 45' W.

240 Angle S. 76° 45' W.

Sta. 244+36.6 Angle S. 89° 00' W.

245. Line between Williams and Grubbs.

B.M. 30' Bench N. 242+50

245+25	9.30			
245+50 T.P.	8.42	116.89	8.42	30
π	1.18	118.07	8.42	5.6
			1.5	23
246 T.P.	7.85	110.22	Level	
π	1.40	111.62	7.85	2.90
			77	30
247 T.P.	11.65	99.99	11.65	14.00
			79	30
π	1.35	101.32	11.65	9.30
			21	30
B.M.	6.47			
248 T.P.	8.40	92.92	8.40	2.60
			15	30
π	1.93	94.85	8.40	4.90
			17	30
248+50 T.P.	7.25	87.57	Level	
π	3.16	90.73	same 295	
249 T.P.	9.35	81.38	9.35	9.60
			79	30
π	1.71	83.09	9.35	6.40
			50	30
249+15 T.P.	8.01	75.08	8.01	11.90
			11	23
π	2.43	77.51	8.01	
			5.56	
			15	
249+90	8.15			
B.M.	7.80			
250 T.P.	8.90	68.64	8.90	12.30
			19	30
π	2.42	71.03	Level	
251 T.P.	8.43	62.60	Level	
π	4.80	67.40	8.43	11.3
			9	15

5' wide  
 Black bridge. Bottom of ditch same  
 slope bottom  
 Sta 250+47 Angle N. 87°-15' W.

B.M. 30" Linn N 247  
 Sta 252+30.6" Angle N. 61° 45' W.  
 (E. of Mad River bridge)  
 Boulders on S. side

Grubb's fireway

Grubb's gate  
 B.M. Grubb N.E. cor. foot stone

251+50	5.10		5.10 6 5.20 7	5.30 28 8.30 16	
252	5.15		5.15 10 5.25 7	7.00 18 11.00 19	
253	4.70		4.70 7 4.70	12.30 28 8.40	9.10 30
B.M.	5.30		5	16	
253+70	4.50				
254 T.P.	5.15	62.25	5.15 7	10.10 20	7.70 30
T	3.66	65.91	5.15 0	9.30 18	7.10 30
255	5.30		5.30 6 5.30	8.00 18 8.30	6.00 30 7.50
256	5.20		5.20 6 5.20 6	8.30 18 8.30 18	7.50 30 7.50 30
257	4.80		same		
258	4.90		"		
259	5.00		"		
259 T.P.	5.37	60.54			
T	5.36	65.90			
260	4.85		4.85 11 4.85 9	7.40 18 7.40 16	6.20 30 6.40 30
261	4.90		same		

Sta. 259+29. T. & O.C. R. R. Switch.

Sta 260+46 Angle N. 62° 00' W.

B.M. N.E. cor. N.E. wingwall of Madriver bag  
E. of Madriver bag, 30' span

Sta 262+30-5" Angle N 90° 15' W

Sta 262+60. @ Wonders lane  
N. side

Sta 263. three nails around  
spike in west plank of bridge  
over Pennock ditch.

Sta 263 Angle N. 88° 15' W

T. & O.C. R.R. switch on E. rail

Sta 267(1)+66 End of pipe  
@ of W. V. Z. & R. pipe  
at Zanesfield.

262	5.40	
262+60	5.30	
B.M.	5.79	
Bot ditch	11.50	
263 T.P.	4.38	61.52
T	9.81	<u>71.33</u>
264	9.10	Level
		"
265	4.90	"
		"
266 T.P.	15.5	69.78
T	6.88	<u>76.66</u>
267	5.60	"
267+66	4.60	
B.M.	3.64	78.02

Weylers Lane  
 B.M. N.E. Stone abut of bridge  
 over Pennock ditch  
 Bank bridge over Pennock ditch  
 Bottom of Pennock ditch

B. W.L. 2 T R. in Jonesfield  
 S. N. S. cor. McAtee door sill in  
 Jonesfield.

12:30  
27/20  
Check Levels

#0		
B.M.		<u>27.95</u>
π	6.03	<u>35.98</u>
4 T.P.	11.05	<u>24.93</u>
π	1.18	<u>26.11</u>
8 T.P.	6.19	<u>19.92</u>
π	9.35	<u>29.27</u>
T.P.	1.51	<u>27.76</u>
π	10.64	<u>38.45</u>
T.P.	1.40	<u>37.05</u>
π	6.73	<u>43.78</u>
T.P.	4.25	<u>39.53</u>
π	12.91	<u>52.44</u>
T.P.	2.28	<u>50.16</u>
π	12.00	<u>62.16</u>
T.P.	0.85	<u>61.31</u>
π	10.44	<u>71.75</u>
19 T.P.	1.55	<u>70.20</u>
π	11.99	<u>82.19</u>
T.P.	1.87	<u>80.32</u>
π	10.23	<u>90.55</u>
T.P.	1.10	<u>89.45</u>
π	11.45	<u>100.90</u>

100.90

T

T.P. 1.93 98.97

T 10.18 109.15

T.P. 7.22 107.93

T 10.25 118.18

T.P. 0.96 117.22

T 11.76 128.98

T.P. 1.60 127.38

T 12.35 139.73

T.P. 0.69 134.04

T 9.02 143.06

T.P. 6.69 149.75

T 8.55 158.30 155.12

T.P. 2.63 153.30

T 11.04 164.34

T.P. 0.73 163.61

T 2.40 166.01

T.P. 2.08 163.93

T 12.87 176.80

T.P. 2.75 174.05

T 10.27 184.32

T.P. 1.41 182.91

T 8.86 191.77

113.93  
2.10  
116.03

191.77

142.97

π

T. P. 0.83 190.94

π 12.34 203.28

T. P. 1.15 202.13

π 11.01 213.14

T. P. 0.64 212.50

π 12.53 225.03

T. P. 0.79 224.24

π 9.45 233.69

T. P. 0.90 232.99

π 9.12 242.11

ST. P. 0.85 241.26 241.25

π 12.34 253.60

T. P. 0.69 252.91

π 11.92 264.83

T. P. 0.67 264.16

π 10.52 274.68

T. P. 1.18 273.50

π 9.80 283.30

T. P. 0.83 282.47

π 10.14 292.61

T. P. 0.69 291.92

π 10.80 302.72



$\pi$	<del>300.90</del>	<u>301.97</u>	
T.P.	0.73	301.97	
$\pi$	2.82	<u>304.99</u>	<u>304.81</u>
T.P.	2.69	302.15	302.17
$\pi$	11.99	<u>314.12</u>	<u>314.14</u>
T.P.	0.68	313.44	313.46
$\pi$	10.00	<u>323.44</u>	<u>323.46</u>
T.P.	2.30	321.14	321.16
$\pi$	11.32	<u>332.46</u>	<u>332.48</u>
T.P.	2.84	329.62	329.64
$\pi$	12.30	<u>341.92</u>	<u>341.94</u>
T.P.	1.26	340.64	340.66
$\pi$	11.55	<u>352.19</u>	<u>352.21</u>
T.P.	1.10	351.09	351.11
$\pi$	8.67	<u>359.76</u>	<u>359.78</u>
T.P.	1.90	357.86	357.88
$\pi$	12.69	<u>370.55</u>	<u>370.57</u>
T.P.	1.73	368.82	368.84
$\pi$	3.51	<u>362.33</u>	<u>372.35</u>
T.P.	10.60	351.73	361.75
$\pi$	1.85	<u>353.58</u>	<u>363.60</u>
T.P.	1.95	351.63	361.65
$\pi$	0.59	<u>352.22</u>	<u>362.24</u>

353

27+27 362.27  
 6.81  
 355.46

<del>T</del>	<del>352.22</del>	<del>352.22</del>	<del>T.P.</del>	<del>6.81</del>	<del>345.41</del>
<del>T</del>	<del>1.85</del>	<del>346.99</del>	<del>T</del>	<del>4.05</del>	<del>349.49</del>
<del>T.P.</del>	<del>12.40</del>	<del>338.89</del>	<del>T.P.</del>	<del>9.28</del>	<del>340.21</del>
<del>T</del>	<del>4.13</del>	<del>338.02</del>	<del>T</del>	<del>1.80</del>	<del>342.01</del>
<del>T.P.</del>	<del>10.46</del>	<del>327.56</del>	<del>T.P.</del>	<del>10.45</del>	<del>331.50</del>
<del>T</del>	<del>1.57</del>	<del>329.43</del>	<del>T</del>	<del>2.08</del>	<del>333.64</del>
<del>T.P.</del>	<del>8.00</del>	<del>321.13</del>	<del>T.P.</del>	<del>11.08</del>	<del>322.56</del>
<del>T</del>	<del>1.51</del>	<del>322.72</del>	<del>T</del>	<del>0.45</del>	<del>323.01</del>
<del>T.P.</del>	<del>10.61</del>	<del>312.12</del>	<del>T.P.</del>	<del>12.10</del>	<del>310.91</del>
<del>T</del>	<del>1.32</del>	<del>313.54</del>	<del>T</del>	<del>0.71</del>	<del>311.62</del>
<del>T.P.</del>	<del>7.42</del>	<del>308.02</del>	<del>T.P.</del>	<del>8.16</del>	<del>303.56</del>
<del>T</del>	<del>1.77</del>	<del>307.79</del>	<del>T</del>	<del>2.37</del>	<del>305.73</del>
<del>T.P.</del>	<del>8.91</del>	<del>298.73</del>	<del>T.P.</del>	<del>8.07</del>	<del>298.86</del>
<del>T</del>	<del>3.80</del>	<del>302.53</del>	<del>T</del>	<del>3.67</del>	<del>302.53</del>
<del>T.P.</del>	<del>2.53</del>	<del>299.67</del>	<del>T.P.</del>	<del>4.47</del>	<del>295.06</del>
<del>T</del>	<del>3.51</del>	<del>301.19</del>	<del>T</del>	<del>2.47</del>	<del>300.53</del>
<del>T.P.</del>	<del>12.40</del>	<del>290.78</del>	<del>T.P.</del>	<del>12.30</del>	<del>288.23</del>
<del>T</del>	<del>0.54</del>	<del>291.32</del>	<del>T</del>	<del>1.61</del>	<del>289.84</del>
<del>T.P.</del>	<del>8.41</del>	<del>281.42</del>	<del>T.P.</del>	<del>8.41</del>	<del>281.43</del>
<del>T</del>	<del>2.02</del>	<del>283.44</del>	<del>T</del>	<del>0.91</del>	<del>282.34</del>
<del>T.P.</del>			<del>T.P.</del>	<del>2.68</del>	<del>274.56</del>
<del>T</del>			<del>T</del>	<del>0.58</del>	<del>275.09</del>

π

275.09

T.P. 12.70 26239

<sup>121</sup>π 1.35 26394 ~~X~~

T.P. 9.28 253.66 ~~X~~

π 0.26 253.92

T.P. 10.99 24293

π 1.70 244.63

T.P. 9.62 235.01

π 0.22 235.23

<sup>234</sup>T.P. 10.61 224.62

π<sub>235</sub> 1.00 225.62

T.P. 9.92 215.70

π<sup>236</sup> 1.46 217.16

T.P. 8.98 208.18

• π<sup>237</sup> 1.38 209.56

T.P. 7.42 202.14

π<sup>238</sup> 1.11 203.25

T.P. 7.64 195.61

π<sup>239</sup> 1.78 196.79

T.P. 9.71 187.06

π<sub>240</sub> 1.26 188.32

T.P. 11.60 176.72

π 1.90 178.62 ✓

$\pi$ 175.65T.P. 12.77 165.65 $\pi$  0.88 166.43T.P. 12.73 153.70 $\pi$  1.84 155.54T.P. 11.31 144.23 $\pi$  3.36 144.59T.P. 11.21 133.32 $\pi$  1.20 134.52T.P. 12.02 122.50 $\pi$  0.96 123.46T.P. 11.86 111.60 $\pi$  0.29 111.89T.P. 7.33 104.56 $\pi$  1.24 105.80T.P. 10.64 95.16 $\pi$  0.68 95.26T.P. 9.65 86.11 $\pi$  2.30 88.41T.P. 4.20 79.24 $\pi$  1.96 81.17T.P. 9.00 72.17 $\pi$  0.97 72.69

T

72.69

T.P 11.43 61.24

T 2.53 64.09

T.P. 8.70 55.39

T 5.07 60.44

T.P 4.85 55.56

T 10.75 66.31

T.P 1.13 65.18

T 5.59 70.77

T.P. BM 3.72 67.05

5.97

85  $\pi$

12.34 - 12.34

86

8.74

85 T.P.

241.07

T	12.34	<u>253.41</u>
86	8.74	
87	4.06	
T.P.	1.19	252.22
T	9.92	<u>262.14</u>
88	4.90	
T.P.	0.25	261.89
T	9.37	<u>271.26</u>
89	5.20	
90	4.80	
91	2.75	
T.P.	1.62	269.64
T	9.31	<u>278.95</u>
B.M.	6.55	272.40
92	6.60	
T.P.	0.10	278.85
T	8.31	<u>287.16</u>
93	6.10	
94	4.70	
95	3.60	
96 T.P.	1.25	285.91
T	10.93	<u>296.84</u>

<del>97</del>	<del>296</del>	<u>296.54</u>	
97	6.70		
98.T.P.	0.17	296.67	
<del>99</del>	<del>5.20</del>	<u>301.87</u>	
99	4.50		
100	5.40		
101	5.20		
102	3.40		
103.T.P.	4.00	297.86	
<del>104</del>	<del>1.10</del>	<u>297.16</u>	
104	3.10		
105	6.56		292.40
To P.	13.15	285.51	
<del>106</del>	<del>0.43</del>	<u>286.29</u>	
106	1.90		284.34
			281.92
107	4.30		287.94
108	8.30		287.44
109	8.80		282.71
110 (peg)	3.53		

185 + 21  
102  
194

100 + 20 Ang. N. 89° 15' W.

108 Ang. N. 87° 15' W.

107 + 27 S. 61° 30' W.

100 + 22 Line Fremma + Piper



243

145.23

π	1.05	<u>146.28</u>
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T.P.	13.04	133.24
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π	0.04	<u>133.28</u>
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244	2.04	
-----	------	--

T.P.	12.81	126.47
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π	0.74	<u>127.21</u>
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245	0.80	
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246 T.P.	11.41	109.80
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π	0.12	<u>109.92</u>
---	------	---------------

197	10.45	<u>99.47</u>
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331.24

12016.1

109.60

99.47

~~243 T.P.~~

<del>π</del>	<del>0.155</del>	<del>146.5</del>
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<del>T.P.</del>	<del>12.00</del>	<del>134.5</del>
-----------------	------------------	------------------

<del>π</del>	<del>0.43</del>	<del>134.93</del>
--------------	-----------------	-------------------

<del>244</del>	<del>3.40</del>	
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<del>T.P.</del>	<del>12.45</del>	<del>127.15</del>
-----------------	------------------	-------------------

<del>π</del>	<del>0.16</del>	<del>127.31</del>
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<del>245</del>	<del>2.70</del>	
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<del>246 T.P.</del>	<del>10.52</del>	<del>116.77</del>
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<del>π</del>	<del>1.21</del>	<del>117.98</del>
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<del>247</del>	<del>11.50</del>	<del>100.48</del>
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~~145.23~~

98.48

20.93

79.97

1.55	
------	--

105.23

13.04

118.28

13.04

133.24

0.04

133.28

12.81

126.47

0.74

127.21

11.41

109.80

0.80

109.92

10.45

99.47

0.12

99.47

111.26

11.04

100.17

99.97

0.20